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nae.	USER'S MANUAL, VERSION 2.0 FOR MONTEBURNS, VERSION 5B
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User's Manual, Version 2.0

for

Monteburns, Version 1.0

September 1, 1999

by

David I. Poston Holly R. Trellue

TABLE OF CONTENTS

1.0 ANTER OR MICHAEL	Page
1.0. INTRODUCTION	2
2.0. REQUIRED USER TRAINING AND/OR BACKGROUND	2
3.0. DESCRIPTION OF MONTEBURNS	3
3.1. Description of <i>Monteburns</i>	
3.2. MCNP Description	8
3.3. ORIGEN2 Description	
3.4. Calculations	
3.4.1. Energy per Fission	14
3.4.2. Flux Tally Normalization/Reactor Physics Constants	
3.4.3. Reactor Physics Constants	1/
3.4.4. Effective Multiplication Factor	
3.4.5. Power	
3.4.6. Fractional Importance	
3.4.7. Activity, Heatload, and Radiotoxicities	20
4.0. USER INTERACTIONS WITH THE SOFTWARE	
4.1. Required Input Files	22
4.2. Main Input Parameters	22
4.3. Feed Input Parameters	29
5.0. DESCRIPTION OF INPUT FILES	
5.1. MCNP Input File	
5.2. Monteburns Input File	
5.3. Feed Input File	
5.3.1. Basic Information	
5.3.2. Feed Information	
5.3.3. Removal Information	
5.3.4. Feed Material Groups	33
5.3.5. Removal Groups	35
5.3.6. Material Shuffling	
5.3.7. Format of Files	
5.3.8. Constant Burn Cases	
5.4. Cross-section Map	
6.0. ERROR MESSAGES	
7.0. OUTPUT FILES	
8.0. LIMITATIONS OF AND FUTURE WORK FOR <i>MONTEBURNS</i>	45
9.1. UNIX	
9.2. PC	
9.3. VMS	
10.0. REFERENCES	
11.0. APPENDICES	50
APPENDIX A - MCNP Input File - test1	
APPENDIX B - Monteburns Input File With No Feed- test1.inp	
APPENDIX C - MCNP Input File - test5	58
APPENDIX D - Monteburns Înput File – test5.inp	
APPENDIX E - Feed Input File – test5.feed	
APPENDIX F - Sample MCNP Cross-section Map - mbxs.inp	

TABLES

TABLE 1	PROCEDURE9)
TABLE 2	SUMMARY OF FILES USED IN MONTEBURNS12	2
TABLE 3	FRACTION OF RECOVERABLE ENERGY PER FISSION FOR CERTAIN	
ACTINI	DES DIVIDED BY THE RECOVERABLE ENERGY PER FISSION FOR ²³⁵ U	
	16	
TABLE 4	INITIAL CROSS-SECTION LIBRARIES PROVIDED BY ORIGEN227	7
TABLE 5	DESCRIPTION OF MONTEBURNS INPUT FILE 31	
TABLE 6a	DESCRIPTION/EXAMPLE 1 OF FEED INPUT FILE	3
TABLE 6b	EXAMPLE 2 OF FEED INPUT FILE)
TABLE 7	ERROR MESSAGES40)
	FIGURES	
FIGURE 1.	Interaction of Monteburns with MCNP and ORIGEN24	ļ
	MONTEBURNS Flow Chart6	
		•

USER'S MANUAL, VERSION 2.0

FOR

MONTEBURNS. VERSION 1.0

by

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ABSTRACT

Monteburns is a fully automated tool that links the Monte Carlo transport code MCNP with the radioactive decay and burnup code ORIGEN2. Monteburns produces a large number of criticality and burnup results based on various material feed/removal specifications, power(s), and time intervals. The program processes input from the user that specifies the system geometry, initial material compositions, feed/removal specifications, and other code-specific parameters. Various results from MCNP, ORIGEN2, and other calculations are then output successively as the code runs. The principle function of monteburns is to transfer one-group cross-section and flux values from MCNP to ORIGEN2, and then transfer the resulting material compositions (after irradiation and/or decay) from ORIGEN2 back to MCNP in a repeated, cyclic fashion. The basic requirement of the code is that the user have a working MCNP input file and other input parameters; all interaction with ORIGEN2 and other calculations are performed by monteburns.

This report serves as a user's manual for monteburns. It describes how the code functions, what input the user must provide, and the calculations performed by the code. It also presents the format required for input files, as well as samples of these files. Monteburns is still in a developmental stage; thus, additions and/or changes may be made over time, and the user's manual will change as well. This is the second version of the user's manual (valid for monteburns previous version 5B, now known officially as Version 1.0); users should contact the authors to inquire if a more recent version is available (Note: for versions of monteburns before and including 4B, users should see the first version of the user's manual).

1

1.0. INTRODUCTION

As computational power continues to increase, it becomes more practical to utilize Monte Carlo methods to perform burnup calculations. *Monteburns* was designed to link the Monte Carlo N-Particle Transport Code (Ref. 1) MCNP and the radioactive decay and burnup code ORIGEN2 (Ref. 2). The primary function of MCNP is to calculate one-group cross-sections and fluxes that are used by ORIGEN2 in burnup calculations as well as provide criticality and neutron economy information if requested. After performing burnup calculations using ORIGEN2, *monteburns* passes isotopic compositions of materials back to MCNP to begin another burnup cycle.

Monteburns consists of a Perl script file that executes MCNP, ORIGEN2, and the FORTRAN77 code monteb.f. Monteburns.pl and monteb.f manipulate the input and output from MCNP and ORIGEN2 to form a completely automated burnup tool. The input to monteburns begins with a working MCNP input file, and its format does not have to be specific. Other input includes material feed and removal information, and other code-specific variables used to perform burnup calculations in ORIGEN2 concurrently with flux/cross-section calculations in MCNP. Final results are reported as a combination of the output from the aforementioned codes. The name monteburns was chosen because it is a Monte Carlo burnup tool.

2.0. REQUIRED USER TRAINING AND/OR BACKGROUND

To run monteburns, a user currently MUST have

- access to a UNIX, PC, or VMS operating system,
- I working versions of MCNP and ORIGEN2 and the corresponding cross-section sets and ORIGEN2 decay information,
- 🛘 a sufficient understanding of MCNP to create a working MCNP input file with desired parameters,
- ullet the ability to compile and/or execute a FORTRAN77 program, and $\ensuremath{\mathbb{I}}$
- I the ability to execute a Perl script file.

MCNP is a trademark of Los Alamos National Laboratory and is available through the Radiation Safety Information Computational Center (RSICC) as code CCC-660.

ORIGEN2 is a popular radioactive decay and buildup code produced by Oak Ridge National Laboratory and distributed by the Radiation Safety Information Computational Center as code CCC-371.

† More information about the Perl language can be found at <u>www.perl.com</u>. Most versions of Perl can then be downloaded from there or www.activestate.com.

3.0. DESCRIPTION OF MONTEBURNS

Monteburns consists of a Perl script file that frequently interacts with a FORTRAN77 program, monteb.f. It is designed to link the Monte Carlo transport code MCNP with the radioactive decay and burnup code ORIGEN2. Monteburns produces a large number of criticality and burnup results based on various material feed/removal specifications, power(s), and time intervals. The program processes input from the user that specifies the system geometry, initial material compositions, feed/removal specifications, and other code-specific parameters. Various results from MCNP, ORIGEN2, and other calculations are then output successively as the code runs.

Monteburns performs one or more MCNP and ORIGEN2 runs for each user-specified time step. The number of MCNP/ORIGEN2 runs per time step is specified by the user (whereas multiple runs per time step increase accuracy, they also significantly increase execution time). The user can also specify continuous or discrete (all at one time) material feed and/or removal at each time step. The results obtained from monteburns are more accurate if long irradiation periods are broken up into smaller lengths of time because the physics and composition of materials in the system may change significantly per unit time. The user can then specify that the time steps be divided into even smaller segments for use in ORIGEN2. This is desirable because smaller time steps often produce more accurate results than longer time steps in ORIGEN2 (especially at the beginning of a system's life) because of differences in computational techniques. In addition, there is virtually no penalty on execution time by using smaller time steps in ORIGEN2 because almost all of the execution time lies with MCNP.

3.1. Description of Monteburns

The primary way in which MCNP and ORIGEN2 interact through monteburns is that MCNP provides one-group microscopic cross-sections and fluxes to ORIGEN2 for burnup calculations. After ORIGEN2 and MCNP have been run, results for each burn step are written into output files, and the isotopic compositions obtained from ORIGEN2 are used to generate a new MCNP input file for the next burn step. This MCNP input file contains the adjusted composition and density of each material being analyzed. To increase the accuracy of the burnup calculation, a "predictor" step is used in which ORIGEN2 is run halfway through the designated burn step. Onegroup cross-sections are then calculated at the midpoint of the burn step by MCNP. This assumes that the isotopics of the system at the midpoint are a reasonable approximation of the isotopics over the entire burn step (actually it is only important that the neutron flux energy spectrum be representative of the entire burn step). The user must be aware of this assumption and consequently ensure that burn intervals are not too long. Monteburns prints out a neutron flux spectrum and the grams of a number of isotopes present for each predictor and each outer burn step in an output file; if there is a large difference between the predictor and the actual burn step, then a shorter burn time should be considered. After the predictor step is executed, then ORIGEN2 is reexecuted with the new one-group cross-sections

(see Section 4.2 for more information). Figure 1 shows how monteburns interacts with MCNP and ORIGEN2.

The other key factor in balancing accuracy with execution time is determining the number of isotopes for which one-group cross-sections should be calculated. For some isotopes it may be important to modify the one-group cross-section, whereas for others, the default ORIGEN2 value may be used with little effect on the solution. Thus, it would be inefficient to calculate a one-group cross-section for every isotope included in the associated MCNP libraries, although this can be done if desired. Isotopes are deemed "important" in two ways. The first way is to explicitly list an isotope in the *monteburns* input file; this insures that one-group cross-sections will be calculated for this isotope during each burn step (and that this isotope will be included in the primary *monteburns* output). The other way in which an isotope is deemed "important" is based on a user input variable called the "importance fraction" (see Section 3.4.6 and/or 4.2 for more information).

There are a number of elements in MCNP for which "natural" cross-sections exist. However, ORIGEN2 does not recognize natural elements, so monteburns contains data to break natural elements into individual isotopes. If a natural cross-section exists in the MCNP input file, monteburns separates this element into its isotopic components, and then ORIGEN2 burns these isotopes individually (with the default ORIGEN2 library cross-sections). After the ORIGEN2 burn, monteburns lumps them back into the common element for use in MCNP. Although this may not be completely correct because ORIGEN2 cross-sections are not modified by MCNP (i.e., and thus not fully representative of the material), it is dictated by the lack of MCNP

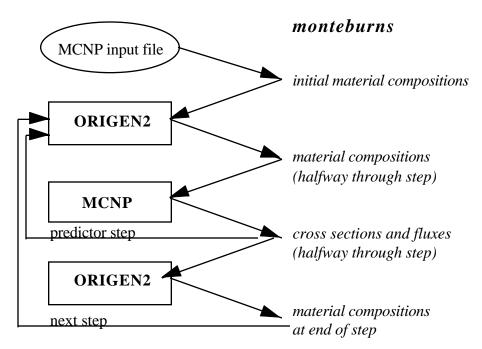


Fig. 1. Interaction of Monteburns with MCNP and ORIGEN2.

cross-sections for many individual isotopes. Whenever possible, it is recommended that the user specify the individual isotopes in the MCNP input file as opposed to using the natural element feature. This allows the isotopics of the element to change as the material burns; it also allows the one-group cross-sections to be modified if any of the isotopes are deemed "important."

The monteburns code does not currently perform any direct temperature-dependent calculations. The user is advised to use a code such as NJOY to process temperature-dependent cross-section libraries, which can then be used by MCNP to process temperature-dependent data. Additionally, monteburns is currently designed to work with MCNP4B, but it also works with MCNP4A and probably any earlier versions as well. Monteburns is also designed to work with either a "kcode"/"ksrc" (criticality) source definition in MCNP¹ or a "sdef"/"src" definition (for other types of transport calculations).

The FORTRAN77 program, *monteb.f*, which interacts with the Perl script file *monteburns.pl*, consists of 15 different parts, each of which performs a different function. These functions are displayed in the detailed flow chart of the Perl script file *monteburns.pl* in Fig. 2, where the numbers correspond to the list below.

- 1. Read input parameters
- 2. Create basic ORIGEN2 input files for each main burn step based on continuous feed/removal information
- 3. Put the user's MCNP input file into monteburns format
- 4. Create tally requests for MCNP
- 5. Write ORIGEN2 composition input file, separating natural elements into individual isotopes
- 6. Update the *monteburns* input file to indicate the current step number and to update the list of isotopes being tracked
- 7. Determine which material is located in each region
- 8. Add discrete feed to ORIGEN2 composition input file (if requested by the user)
- 9. Modify the previous MCNP input file with new material compositions
- 10. Modify ORIGEN2 input files for predictor steps to calculate compositions halfway through each burn step
- 11. Modify ORIGEN2 libraries with cross-sections calculated by MCNP and ORIGEN2 input files with fluxes from MCNP

5

Versions of NJOY are available at the Radiation Safety Information Computational Center (RSICC) as codes PSR-171 and PSR-355.

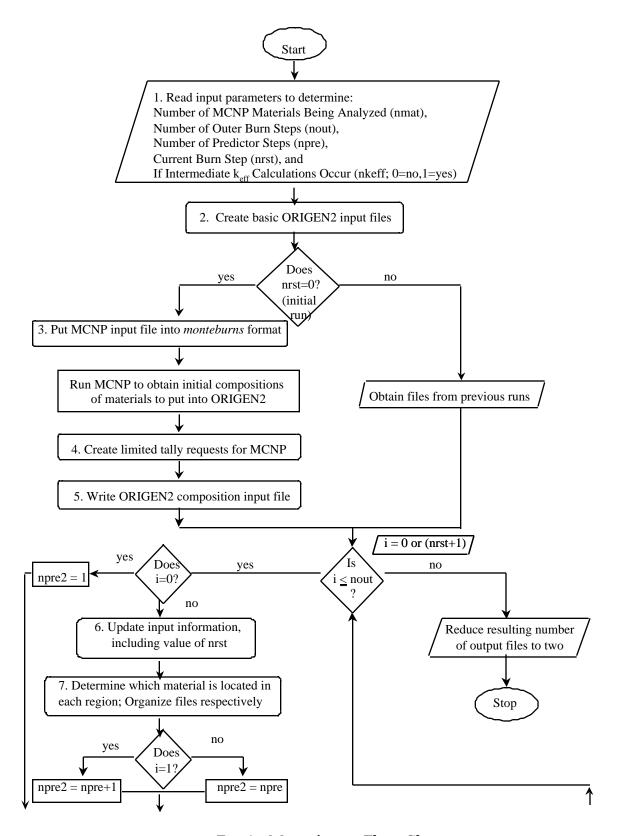


Fig. 2. Monteburns Flow Chart.

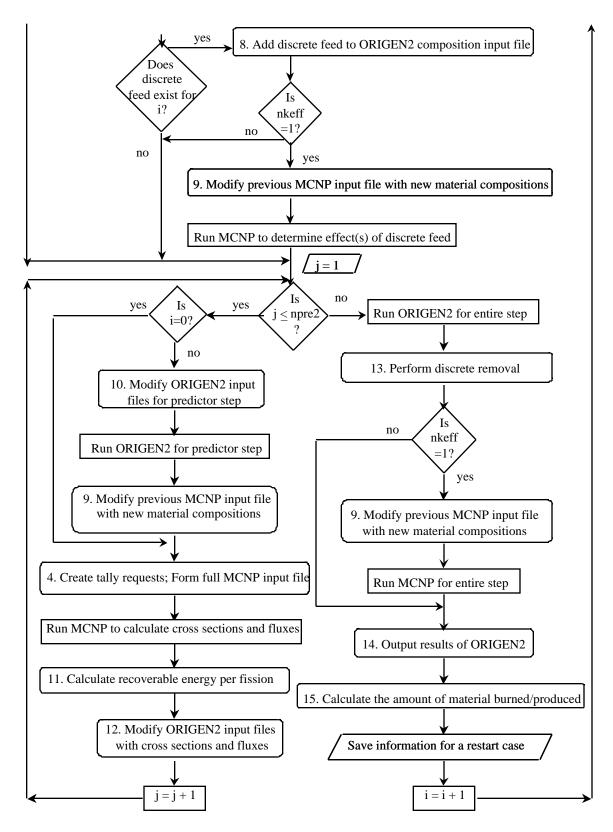


Fig. 2. Monteburns Flow Chart (cont).

- 12. Calculate the recoverable energy per fission based on the actinide distribution
- 13. Perform discrete removal in the ORIGEN2 composition input file
- 14. Output results of ORIGEN2
- 15. Calculate the amount of material burned and produced based on feed and inventory information

Table 1 describes the procedure followed in the execution of *monteburns* (excluding the file management steps) where *** is the base name of the various input files associated with *monteburns*, and # is the number of the current outer burn step. Note: VMS requires a *.dat extension on many files without extensions (primarily input and output from MCNP; therefore, these are included in parentheses where applicable. Table 2 then summarizes the function of each file used in *monteburns*.

Overall, monteburns acts as a pre- and postprocessor for both MCNP4B and ORIGEN2. Although the program is fully automated (except for the creation of input files), it is advised that the user be familiar with nuclear terminology, decay and burnup codes, and Monte Carlo codes such as MCNP to understand the output and to verify that the correct data were obtained.

3.2. MCNP Description

MCNP is a neutral particle transport code that uses the Monte Carlo technique. The Monte Carlo technique is a statistical method in which estimates for system characteristics are obtained through multiple computer simulations of the behavior of individual particles in a system. A Monte Carlo code generates such a statistical history for a particle based on random samples from probability distributions. These distributions are used in calculations to determine the type of interaction the particle undergoes at each point in its life, the resulting energy of the particle if it scatters, the number of particles that "leak" from the system because of geometry constraints, and the number of neutrons produced if the neutron causes a fission. The probability of the particle to behave in a certain manner (scatter, absorb, fission) can be obtained from the cross-section values of the material(s) with which the particle will interact. Thus, a Monte Carlo code can model the series of events that occur in the lives of a large number of particles to determine the flux of different types of particles in various regions in a system. These fluxes can then be used to tally a wide variety of information (reaction rates, heating rates, doses, etc.) for the system. Additionally, the value of the effective multiplication factor, k_{eff} , for a system (the ratio of the number neutrons in the system a particular time to the number of neutrons that existed in the previous generation) can be calculated using MCNP.

TABLE 1 PROCEDURE

Step	Process	Input ^a	Output ^a
1	Read input parameters from	***.inp = mb.inp	mb.inp
	***.inp input file (the primary	tmpfile/params	
	monteburns input file – mb a)		
2	Write natural element file	-	natelem
	(monteb e)		
3	Create ORIGEN2 input files	***.feed = feed	tmpfile/TAPE5_\$.I#
	for each burn step (monteb 5)	orig21/Decay.lib =	TAPE9_0.INP
		ORIGEN2 decay lib.	mb9.txt
		Orig**/^^^.lib =	mb9t_\$.out
		ORIGEN2 cross	tmpfile/params2
		section library	
		(**=ID#/^^^=name)	
	NA LIC MACNID	tmpfile/param_\$.#	1 (1.1)
4	Modify MCNP input file to	***	mbmc(.dat)
	include commands specific to		mbmc.skl
	monteburns (monteb 1)		mat_\$.inp
			mb*.txt (* = 1 to 17)
5	Run the MCNP input	*** = mbmc	mb*t_\$.out (*=11,13)
3	processor on the initial MCNP	= mome	mbmcm (optional) mbmco (.dat)
	input file to obtain the initial		mbmcr (.dat)
	composition of the materials		mbmcs (.dat)
	to be burned		momes (.dat)
6	Create flux tally descriptions	mbmco(.dat)	tal2_\$.inp
	for MCNP input file	indireo (raac)	mb6t_\$.out
	(monteb 2)		
7	Write ORIGEN2 composition	mbmco(.dat)	TAPE7_\$.OUT
	input file, fort.7 based on	mbxs.inp	mnat_\$.tmp
	initial MCNP deck, and	natelem	mcnp_\$.inp
	separate natural isotopes from		
	non-actinides and other		
	isotopes (monteb 4)		_
8	For a restart case, obtain files	tmpfile/TAPE9_\$.I#	TAPE9_\$.INP
	from previous runs	tmpfile/TAPE7_\$.O#	TAPE7_\$.OOU
		tmpfile/TAPE5_\$.I#	tmpfile/TAPE5_\$.t#
		tmpfile/mbmc.#	mbmc(.dat)
2001	lassing assembals amply for the tables # _ mumb	tmpfile/mbinp.#	mb.inp

^aThe following symbols apply for the table: # = number of the current outer burn step, \$ = monteburns material number of current material being analyzed [may or may not be equal to MCNP material number (see Section 5.2 for more information)], **** = base names of files, and @ = the number 1–17.

TABLE 1 (cont) PROCEDURE

Step	Process	Input ^a	Output ^a
9	Determine which material is	tmpfile/params2	tmpfile/para3_\$
	in each region and organize	feed	
	files respectively	tmpfile/TAPE5_\$.t#	tmpfile/TAPE5_\$.I#
		mnat_\$.tmp	mnat_\$.tmp
10		TAPE7_\$.OUT	TAPE7_\$.OUT
10	Rewrite input information,	***.inp = mb.inp	mb.inp
	including number of outer steps currently being processed	tmpfile/param_\$.#	
	(monteb 9). Determine if		
	discrete feed exists or not		
11	Add discrete feed to ORIGEN2	TAPE7_\$.OUT	TAPE7_\$.TMP
	composition input file	tmpfile/params2	tmpfile/param_\$.#
	(monteb b)	feed	tape.tmp
	,	natelem	1 1
12	Modify previous MCNP input	TAPE7_\$.OUT	mb7_\$.out
	file by adding discrete feed	TAPE9_\$.INP	mat_\$.inp
	(monteb 7b)	mbxs.inp	tmpfile/T9err_\$.TXT
		mcnp_\$.inp	
10		mnat_\$.tmp	mbmc.skl
13	Run MCNP to determine	mbmc.skl	mbmco(.dat)
14	effect(s) of discrete feed	mat_\$.inp	b11 Ct
14	Obtain criticality values from MCNP output file (monteb 6b)	mbmco(.dat)	mb11_\$.out
	MCNF output the (montes ob)	tmpfile/params2 feed	
15	Output results (monteb 8b)	TAPE7_\$.OUT	mb5\$.out
16	Run ORIGEN2 for predictor	tmpfile/TAPE5_\$.#	TAPE6.OUT
	step(s) (i.e., halfway through	= TAPE5_\$.INP	TAPE7_\$.TEM =
	each step)	TAPE4_\$.INP	TAPE7_\$.OUT
	1,	TAPE9_\$.INP	
		tmpfile/params2	
		feed	
17	Modify previous MCNP input	TAPE7_\$.OUT	mb4_\$.out
	file by adding new	TAPE9_\$.INP	mb7_\$.out
	compositions, and tally	mbxs.inp	mat_\$.inp
	isotopes if deemed	mcnp_\$.inp	tmpfile/T9err_\$.TXT
10	"important" (monteb 7m)	mnat_\$.tmp	mbmc.skl
18	Create full MCNP input file	mbmc.skl	mbmc(.dat)
	from user-generated version,	mat_\$.inp	
	including tallies (monteb 3)	tal1-3_\$.inp	

TABLE 1 (cont) PROCEDURE

Step	Process	Input ^a	Output ^a
19	Run MCNP to calculate one-	mbmc(.dat)	mbmco(.dat)
	group cross-sections and		
	fluxes		
20	Modify ORIGEN2 file with	feed	mb1-3,6,8,14-17_\$.out
	new cross-section and flux	mbmco	mb11.out
	values obtained by MCNP	TAPE7_\$.OUT	tmpfile/mtu_\$.tmp
	(monteb 6m)	TAPE9_\$.INP	TAPE9_\$.INP
		tmpfile/TAPE5_\$.#	tmpfile/TAPE5_\$.t#
		tmpfile/params2	
21	Run ORIGEN2 for entire step.	tmpfile/TAPE5_\$.#	TAPE6.OUT
	Print results halfway to	= TAPE5_\$.INP	$TAPE7_{}TEM =$
	compare with predictor step(s)	TAPE4_\$.INP	TAPE7_\$.OUT
	and then perform discrete	TAPE9_\$.INP	mb14-17_\$.out
	removal (includes monteb 8e	tmpfile/params2	mb5\$.out
	and two ORIGEN2 runs)	feed	
00		mbmco(.dat)	. C1 /EADEO 6 "
22	Save information for a restart	TAPE9_\$.INP	tmpfile/TAPE9_\$.#
	case	TAPE7_\$.OUT	tmpfile/TAPE7_\$.#
		mbmc(.dat)	tmpfile/mbmc.#
23	Modify provious MCND input	mb.inp TAPE7_\$.OUT	tmpfile/mbinp.# mb7_\$.out
23	Modify previous MCNP input file by adding new	TAPE7_\$.OUT	mat_\$.inp
	compositions of materials	mbxs.inp	tmpfile/T9err_\$.TXT
	(monteb 7e)	mcnp_\$.inp	unpine/13en_ş.1X1
	(monted /e)	mnat_\$.tmp	
24	Run MCNP for complete	mbmc.skl	mbmco(.dat)
~ -	outer step	mat_\$.inp	momeo (raat)
25	Obtain criticality values from	mbmco(.dat)	mb11_\$.out
	MCNP output file (monteb 6e)	tmpfile/params2	
	, , , , , , , , , , , , , , , , , , ,	feed	
26	Remove discrete removal	tmpfile/params2	tmpfile/TAPE7_\$.O#
	group elements (monteb d)	feed	-
		TAPE7_\$.OUT	
27	Output results of ORIGEN2	mbmco(.dat)	mb14-17_\$.out
	(monteb 8e)	TAPE7_\$.OUT	mb5\$.out
		TAPE9_\$.INP	

TABLE 1 (cont) PROCEDURE

Step	Process	Input ^a	Output ^a
28	Calculate the amount of	mb5t_\$.out	mb9_\$.out
	material burned and produced	mb5tx_\$.out	mb9t_\$.out
	based on feed and inventory	mb12a_\$.out	mb10.txt
	information	mb9t_\$.out	mb10t_\$.out
	(monteb z)	tmpfile/params2	
29	Reduce resulting number of	mb@t_\$.out	***.chk
	input files to two	mb@.txt	***.out

TABLE 2 SUMMARY OF FILES USED IN MONTEBURNS

File	Description a,b
***	MCNP input file created by user (user can choose any name ***
mbmc	that meets MCNP requirements: i.e., no more than 7 characters)
	Name of MCNP input file used by monteburns (initially = ***)
	Skeleton MCNP input file (based on ***)
mbmc.skl	Name of MCNP input files saved for restart runs (# = outer burn
/tmpfile/mbmc.#	step)
mat_\$.inp	Contains modified MCNP material cards after each burn step
tal1_\$.inp	These three files contain commands that are used to generate the
tal2_\$.inp	flux spectrum, cross-section, and other tallies in MCNP. These
tal3_\$.inp	files are merged with the MCNP input file before MCNP is run
_	(except for intermediate criticality only runs).
mbxs.inp	This file lists the default MCNP cross-section library to be used
_	for each isotope if is not already identified.
mbmco	Default name of MCNP output files
mbmcr	-
mbmcs	
***.feed	Optional input file created by user, contains feed/removal and
	time-step information
feed	Name of default feed file used in monteburns (initially = ***.feed)
***.inp	Input file created by user, contains code specific variables
mb.inp	Name of default input file used in monteburns (initially = ***.inp)
tmpfile/mbinp.#	Name of input files saved for restart runs
TAPE9_\$.INP	Contains values from the ORIGEN2 decay and cross-section
TAPE9_\$.TMP	libraries. This file goes through various temporary stages, which
TAPE9_0.INP	include replacing ORIGEN2 cross-section values with ones
tmpfile/TAPE9_\$.I#	obtained from MCNP. The variations listed to the left represent
	the temporary files, the last of which is used for restart runs

^aThe bolded file names represent those supplied by the user.

^bThe following symbols apply for the table: # = number of current outer burn step, \$ = number of current material being analyzed, *** = base name of files.

TABLE 2 (cont) SUMMARY OF FILES USED IN MONTEBURNS

File	Description a, b
tmpfile/T9err_\$	Displays errors incurred from finding cross-section values in
	fort_\$.9
TAPE4_\$.INP	Contains the names of isotopes and their number densities that
TAPE7_\$.OUT	will be processed in ORIGEN2, units are in gram-atoms (fort.4 =
TAPE7_\$.TMP	ORIGEN2 input, fort.7 = ORIGEN2 output, $\#$ = outer burn step)
TAPE7_\$.TEM	
tmpfile/TAPE7_\$.O#	
orig21/Decay.lib	'orig21' is the identifier of the ORIGEN2 decay library
orig##/^^^.lib	## then identifies the cross-section library requested by the user
	or ^^^ is the name
mcnp_\$.inp	Contains a list of isotopes/elements in the initial MCNP input
	file
mnat_\$.tmp	Contains a list of natural elements from the initial MCNP input
	file
TAPE5_\$.INP	Working ORIGEN2 input file
TAPE5_\$.TMP	Temporary ORIGEN2 input files (# = outer burn step)
/tmpfile/TAPE5_\$.#I	
TAPE6.OUT	Working ORIGEN2 output file
tmpfile/params	Temporary files used by monteburns to read input parameters
tmpfile/params2	and to determine if discrete feed exists or not for each outer burn
tmpfile/para3_\$	step (#).
tmpfile/param_\$.#	
tape.tmp	Below: Individual output files from monteburns
mb1.txt&mb1t_\$.out,	mcnp results: k _{eff} , nu,flux, variance, and cross-sections
mb2.txt&mb2t_\$.out,	n,gamma for automatic and important isotopes
mb3.txt&mb3t_\$.out,	n, fission for tracked isotopes
mb4a.txt&mb4a_\$.out,	spectrum for predictor steps
mb4b.txt&mb4b_\$.out,	inventory of tracked isotopes at halfstep (predicted)
mb5.txt,mb5t_\$.out,	inventory of tracked isotopes at halfstep (actual)
mb5x_\$.out	inventory of tracked isotopes at halfstep (with precision for
&mb5tx_\$.out	more calc)
mb6.txt&mb6t_\$.out,	flux spectrum during steps
mb7.txt&mb7t_\$.out,	materials sent back to mcnp each time it is run
mb8.txt&mb8t_\$.out,	fission-to-capture ratio
mb9.txt&mb9t_\$.out,	feed and burnup of tracked isotopes, total actinide, and final
mb10.txt&mb10_\$.outmb	summary feed and burnup rates
11t \$.out	men results: day (time of cumulative irradiation), k_{eff} , and
111_3.0ut	variance $\frac{1}{2}$
mb12.txt&mb12t_\$.out	inventory of materials at the beginning of each step
mb12x&mb12tx_\$.out	beginning inventory (with greater precision)
mb13t \$.out	k _{eff} at beginning of each step
mb14.txt,mb14t_\$.out	activity of tracked isotopes at end of step (Ci)
mb15.txt,mb15t_\$.out	heatload of tracked isotopes at end of step (W)
mb16.txt,mb16t \$.out	inhalation toxicity of isotopes at end of step (m ³ air)
mb17.txt,mb17t_\$.out	ingestion toxicity of isotopes at end of step (m³ water)
***.chk, ***.out	Final output files from monteburns
icin, iout	That output thes from montenants

3.3. ORIGEN2 Description

ORIGEN2 performs burnup calculations for *monteburns* using the matrix exponential method.² ORIGEN2 considers time-dependent formulation, destruction, and decay concurrently.³ These calculations require (1) the initial compositions and amounts of material, (2) one-group microscopic cross-sections for each isotope, (3) material feed and removal rates (if desired), (4) the length of the irradiation period(s), and (5) the flux or power of the irradiation. The user must give this information in the input files discussed in Section 5.0.

Input files for ORIGEN2 are complicated to write, and output files generated by ORIGEN2 are bulky and complicated to read. Thus, monteburns eliminates the user's need to create his/her own ORIGEN2 input files and to extract information from ORIGEN2 output files. Monteburns provides a "cross-section and decay information" file, TAPE9.INP; a file with material compositions, TAPE4.INP; and a skeleton ORIGEN2 file, TAPE5.INP, which contains commands and continuous feed and removal information.

3.4. Calculations

A number of calculations are performed by *monteburns*. They are divided into six different categories and are presented below. These categories are (1) energy per fission, (2) flux normalization, (3) reactor physics constants, (4) effective multiplication factor, (5) power, and (6) fractional importance.

3.4.1. Energy per Fission

The user has two options of how to calculate the amount of energy deposited per fission for a system. First, he/she can enter the desired Q-value (the average for the entire system) into the *monteburns* input file. Second, the user can enter a Q-value for ²³⁵U that he/she thinks is most representative of the nuclear system being evaluated (preceded by a negative sign in the input file. The code will calculate the average Q. In this case, the following equations are used by *monteburns* to calculate the amount of energy per fission for each material [see Eq. (4) for the Q-value for the entire system] according to the distribution of various actinides in the material.

The value of Q entered must include all modes of energy deposition, including fission gammas, capture gammas, and neutron kinetic energy. It would be more accurate to run MCNP in the "nps" mode and tally energy deposition, but this would require considerably more computation time. The current method should be sufficiently accurate except in cases where (n,) heating varies significantly as the isotopes of the system change. Future code modifications may address this issue.

$$Q_{fis} = \left| Q_{U-235} \right| * Q_{rat} \quad , \tag{1}$$

where

Q_{fs} =total amount of recoverable energy produced per fission,

 $Q^{235}_{U.}$ =recoverable energy per fission for ^{235}U [input by user-recommended value is 200 MeV (Ref 4)], and

 Q_{rat} =weighting factor to include recoverable fission energy for all actinides present;

$$= \sum_{i=1}^{n} q_{rat}(i) * f_{rat}(i) , \qquad (2)$$

where

n = number of isotopes being considered,

 $q_{rat}(i)$ = ratio of recoverable energy per fission for isotope i divided by the recoverable energy per fission for 235 U (Ref 5) and listed in Table 3, and

 $f_{rat}(i)$ =ratio of fissions resulting from isotope i to total number of fissions [see Eq. (3)];

$$=\frac{f(i)*n(i)}{\binom{n}{f(i)*n(i)}},$$
(3)

where

f(i) = one-group microscopic fission cross-section of isotope, and

n(i) = number density of isotope i in the system (in units of gram-atoms).

TABLE 3 FRACTION OF RECOVERABLE ENERGY PER FISSION FOR CERTAIN ACTINIDES DIVIDED BY THE RECOVERABLE ENERGY PER FISSION FOR 235 U

Isotope	Fraction	Isotope	Fraction
²²⁷ Th	0.9043	²⁴⁰ Pu	1.0379
²²⁹ Th	0.9247	²⁴¹ Pu	1.0536
²³² Th	0.9573	²⁴² Pu	1.0583
²³¹ Pa	0.9471	²⁴¹ Am	1.0513
²³³ Pa	0.9850	^{242m} Am	1.0609
$^{232}{ m U}$	0.9553	²⁴³ Am	1.0685
²³³ U	0.9881	²⁴² Cm	1.0583
$^{234}{ m U}$	0.9774	²⁴³ Cm	1.0685
$^{235}{ m U}$	1.0000	²⁴⁴ Cm	1.0787
$^{236}{ m U}$	0.9973	²⁴⁵ Cm	1.0889
$^{237}\mathrm{U}$	1.0074	²⁴⁶ Cm	1.0991
$^{238}{ m U}$	1.0175	²⁴⁸ Cm	1.1195
²³⁷ Np	1.0073	²⁴⁹ Cm	1.1296
²³⁸ Np	1.0175	²⁵¹ Cf	1.1501
²³⁸ Pu	1.0175	²⁵⁴ Es	1.1807
²³⁹ Pu	1.0435		

Next, the average energy deposited per fission in the system as a whole can be calculated.

$$Q_{\text{ave}} = \frac{\prod_{j=1}^{m} (Q^{j} * j * j * V^{j})}{\prod_{j=1}^{m} (j * j * V^{j})} , \qquad (4)$$

where

 Q_{ave} = the average recoverable energy per fission for all materials, Q_{fis}^{j} = average energy per fission for material j (MeV),

 $_{n}^{j}$ = value of flux of material j obtained from MCNP output file,

= macroscopic fission cross-section of material j (cm⁻¹),

 V^{j} = total volume of all cells containing material j (cm³), and

= number of materials being analyzed

3.4.2. Flux Tally Normalization/Reactor Physics Constants

For each material j, the value of the flux that is used for burnup calculations in ORIGEN2 is calculated from the flux tallied by MCNP (which is normalized per MCNP source neutron):

$$= {}_{n} {}^{*} C , \qquad (5)$$

where

true value of the flux (normalized to system power), and
 a constant [see Eqs. (7) or (9)].

When an MCNP input file with a "kcode" (criticality) source definition is used and k_{eff} and its associated error are found from the MCNP output file, then the value of C is as follows:

$$C = \frac{* P * 10^{6} W/MW}{(1.602 \times 10^{-13} J/MeV) * k_{eff} * Q_{ave}} ,$$
 (6)

where

average number of neutrons produced per fission (see the next section for calculation of),

P = power defined by user for each material (in MW), and

 \mathbf{k}_{eff} = effective multiplication factor obtained by MCNP.

When the MCNP input is a "sdef" source definition, then the value of C is instead

$$C = \frac{\text{src} * P * 10^{6} \text{ W/MW}}{\text{floss} * (1.602 \times 10^{-13} \text{ J/MeV}) * Q_{\text{ave}}} ,$$
 (7)

where

src = weight of source neutrons (approximately equal to one), and
floss= weight of neutrons lost to fission.

3.4.3. Reactor Physics Constants

For both types of source definitions, the value of can be calculated from results in the MCNP output file. For a "kcode" source definition, is calculated as follows:

$$= k_{eff} * src/floss$$
, (8)

where

src = weight of source neutrons (approximately equal to one), and
floss= weight of neutrons lost to fission.

For a "sdef" source definition, the value of is

$$= fsrc/floss$$
, (9)

where

fsrc = weight of source neutrons gained in fission.

For either type of MCNP input file, the number of neutrons produced per neutron destroyed () is

$$=\frac{(f+2.0* n2n+3.0* n3n)}{(a+f)},$$
(10)

where

f = fission cross-section from MCNP,

= (n,) cross-section from MCNP,

 $_{n^{2n}} = (n,2n)$ cross-section from MCNP,

 $_{n3n}$ = (n,3n) cross-section from MCNP, and

= total absorption cross-section from MCNP (-2 reaction tally type).

3.4.4. Effective Multiplication Factor

The value of the effective multiplication factor for an "sdef" source definition must be calculated from the value of the net multiplication obtained from the MCNP output file:

$$k_{eff} = \underline{\text{(fmult - 1)}}$$

$$\text{(fmult - 1/)} ,$$

where

fmult = net multiplication in the system.

The relative error () associated with $k_{\mbox{\tiny eff}}$ is then

$$= \frac{(\text{fmult}^*(1+\text{err}) - 1) - k_{\text{eff}}}{(\text{fmult}^*(1+\text{err}) - 1/)},$$
(12)

where

err = relative error associated with the net multiplication in the system.

3.4.5. **Power**

Finally, the power produced by each material is

$$P^{j} = \underbrace{(Q_{ave} * j * j * J_{f} * V_{J} * 1.60219 * 10^{-13} J/MeV)}_{10^{6} W/MW} , \qquad (13)$$

where

 P^{j} =power produced by material j (MW), and j =flux of neutrons in material j (n/cm²/sec).

3.4.6. Fractional Importance

The fractional importance calculations help determine which isotopes are considered "important" to the overall burnup calculation and which are not. If any of the following values (atom fraction, weight fraction, fraction of absorption, and fraction of fission) are greater than the value of the "fractional importance" assigned by the user, then the isotope is considered "important" and is included in all transfers from ORIGEN2 to MCNP and back throughout the remainder of the run (see Section 4.2 for more information).

$$a_{fi} = \frac{gad_i}{n} ,$$

$$gad_i$$

$$i=1$$
(14)

$$w_{fi} = \frac{gad_i * A_i}{n},$$

$$(gad_i * A_i)$$

$$_{i=1}$$

$$(15)$$

$$f(a)_i = \frac{gad_i * a_i}{n}, \qquad (16)$$

LA-UR-99-4999

and

$$f(f)_i = \frac{gad_i * f}{n}, \qquad (17)$$

$$(gad_i * f)$$

where

i = isotope being studied,

n = total number of isotopes in system,

 a_{fi} = atom fraction of isotope i in system,

 w_{fi} = weight fraction of isotope i in system,

f(_a)_i = fraction of absorption isotope i contributes to system,

 $f(\theta)_i = fraction of fission isotope i contributes to system,$

gad_i = amount of isotope in system in gram-atoms,

A_i = atomic weight of isotope i in grams,

 $_{ai}$ = microscopic absorption cross-section of isotope i, and

= microscopic fission cross-section of isotope i.

3.4.7. Activity, Heatload, and Radiotoxicities

When studying radioactive waste and waste repositories (as well as other applications), it is important to keep track of many things beyond the grams of material at the beginning and end of each burnup step. In fact, some of the most important quantities to calculate are the activity of isotopes in each material as a function of burnup (activation in Curies), the heatload (decay power in Watts), and inhalation and ingestion radiotoxicities (m³ in air and water, respectively).

The following equations are used in monteburns to calculate activity, heatload, inhalation, and ingestion toxicities respectively.

$$Act = m * SA ag{18}$$

and

$$SA = \frac{\ln(2) * N_a}{A * T_{1/2}/3.7 * 10^{10} Bq/Ci} ,$$
 (19)

where

Act = activity of isotope in Ci,

SA =specific activity (Ci/g [activity per gram of material (Ref. 7)],

m =mass of nuclide (g/mole),

 N_a = Avogadro's number = 6.022*10²³ atoms/mole,

A = atomic weight of nuclide (g),

 $T_{1/2}$ = half-life of nuclide (s), and

Bq = disintegrations/s (assume one atom/disintegration).

$$HL = Act *3.7*10^{10} Bq / Ci * Q_{rec} *10^{6} eV / MeV *1.6012*10^{-19} J / eV$$
 (20)

where

HL = heatload (decay power) released by isotope (W), and

 Q_{rec} = average recoverable energy emitted from decay events (MeV), (values obtained from ORIGEN2 decay library).

$$InhTox = \frac{\ln 2 * N}{T_{1/2} * C_{inh}} \tag{21}$$

and

$$IngTox = \frac{\ln 2 * N}{T_{1/2} * C_{ing}}$$
 , (22)

where

InhTox = inhalation toxicity of nuclide (m³ air),

IngTox = ingestion toxicity of nuclide (m³ water),

N = number of atoms of nuclide, and

C = radioactivity concentration limit (Ref. 6).

4.0. USER INTERACTIONS WITH THE SOFTWARE

The primary role of the user in this program is to create the required two to four input files. A description of input parameters is presented below, and the format of the input files is shown in Section 5.0.

4.1. Required Input Files

The user must generate two to four different input files before executing monteburns. The two required input files are the MCNP input file (designated here by mbfile, but can be any name up to 8 characters), and a general monteburns input file (this must have the same prefix "mbfile" with an extension of ".inp" for a name of mbfile.inp). For many complex burnup scenarios, the user must also generate a feed input file (with a name of mbfile.feed), which contains detailed instructions for monteburns at each time step (i.e., time interval, power, and material feed/removal). The only case in which a feed input file is not required is for a constant power burn with no material feed or removal. Finally, monteburns uses one other input file, mbxs.inp, which contains a list of default MCNP cross-section identifiers for isotopes that may be produced in the irradiation process and are not initially specified by the user. A sample of this file is included with the monteburns source code package; this sample file can be modified as requirements dictate (see Section 5.4 for more information).

4.2. Main Input Parameters

The user is required to know many input variables to run this code. The parameters are described below; Section 5.0 discusses how each of these parameters is entered into input files.

- Number of MCNP materials—this indicates the number of materials the user wants to irradiate from the MCNP input file (i.e., transfer back and forth between MCNP and ORIGEN2). Note: The current limit on the number of materials is 49.
- MCNP material number(s)—the identification number of the material(s) in the MCNP input file for which a burnup analysis is desired (monteburns will tally average results over all cells and parts of a repeated structure or lattice that contain this material). If a user desires to obtain information for a material (i.e., flux, cross-sections, etc.) without burning the material in ORIGEN2, then he/she can enter the number of that material here preceded by a negative sign to indicate that it will not be irradiated (however, that material will still be decayed in ORIGEN2). Note: the number of entries here must equal the number of MCNP materials entered above. Additionally, the order in which these material numbers are listed define what monteburns material number is assigned to each MCNP material number (this will be used for determining what material is in each region—see Section 5.3 for more information). For example, if MCNP material 1 is listed first followed by 5 and 10, then monteburns material 1 is initially defined to be MCNP material 1, monteburns material number 2 is MCNP material 5, and monteburns material number 3 is initially comprised of MCNP material 10.

- Material volume(s)—the sum of the volume (cm³) of all cells in the MCNP input file for each material number(s) listed above (again, the number of entries must equal the number of MCNP materials). If the user enters a value of 0.0 for one or more of these, then the volume calculated by MCNP is used (if it exists). However, often the geometry is too complex for MCNP to calculate the volume. In this case, unless the user has input a non-zero volume for that material number, an error message appears, monteburns terminates, and it must be rerun with non-zero values. Additionally, in most cases of repeated structures, MCNP calculates the volume of cells containing a given material incorrectly. For each of these cases (and for any other instances the user desires), the user must enter the sum of the volumes of cells containing each material being analyzed.
- Total power of the system—the power (MW) generated by the entire system represented in the MCNP model (this is not necessarily the same as the power generated solely by the materials burned in monteburns). This value, along with the recoverable energy per fission, is used to normalize the flux from MCNP in each burned region for ORIGEN2. Additionally, the user can enter the fraction of this power to be used during each outer burn step (if power is not constant over the entire burn) in the feed input file. By entering a power fraction of zero for a step, it effectively becomes a decay-only step, which is useful for analyzing cooling periods of systems. Note: the value of fission power output is subject to statistical errors and may not be exactly the same as the power input. Increased statistics in MCNP may minimize this problem; nonetheless, the user should check the value of power output to ensure that it is close to the amount of power initially desired.
- Recoverable energy per fission—this value represents the average recoverable energy per fission (Q) in MeV in the aforementioned MCNP model. If the user does not know the exact amount of energy generated by a combination of several isotopes, then he/she can enter the recoverable energy per fission for ²³⁵U for that system (commonly ~200 MeV for lightwater reactors), preceded by a negative sign. The negative sign means that the value of the recoverable energy per fission will be calculated by monteburns based on the fissile isotopics of the system. In this case, Q is calculated as the sum of all actinide Q fractions, which are based on the fraction of fissions caused by a specific isotope times the Q of that isotope divided by the Q of ²³⁵U (see Eqs. 1-4 for more information). WARNING: the fissile isotopics used for the calculation of Q are based only on the materials burned by monteburns. If the fissile isotopics of the entire system are significantly different from the fissile isotopics of the materials being burned, then the average value of Q may be in error. Thus, the flux normalization may be in error (although in most cases, this should be a relatively small effect).

- Total number of days burned—this number represents the length of time for which a material is irradiated in ORIGEN2 (or the decay time if the power equals zero). If the user provides a feed input file, then the irradiation lengths (in days) for each outer burn step (described below) must be provided in this file and a value of 0.0 entered in the monteburns input file. Otherwise, the total irradiation time (in days) must be entered in the monteburns input file.
- Number of outer burn steps—this number indicates how many outer burn steps are desired. If a feed input file exists, this must equal the number of steps described in the feed input file. If a feed input file does not exist, the length of the irradiation period for each outer burn step equals the total days burned divided by the number of outer burn steps. Each of these steps represents a time period for which a burnup calculation is performed, and representative cross-sections are obtained (the burn step then uses spectrum-averaged, one-group, cross-sections calculated at a predictor step halfway through that step). Each outer step can also indicate the addition and/or removal of a material.
- Number of internal burn steps—this is the number of additional times into which the irradiation period is divided for ORIGEN2 calculations. As mentioned in Section 3.0, the results obtained from ORIGEN2 (and as a result, monteburns) may be more accurate if long irradiation periods are broken up into smaller lengths of time, especially at the beginning of a system's life. This is because the Bateman equations are used instead of the Gauss-Seidel iterative technique to solve for compositions of materials when the half-life of an isotope is <10% of the irradiation interval. Therefore, results may vary according to which technique is used. Additionally, the physics and composition of materials in the system may change significantly with time. Thus, the user can specify that the outer burn steps be divided into even smaller time segments for use in ORIGEN2. In addition, there is virtually no penalty on execution time by using smaller time steps in ORIGEN2 because most of the execution time lies with MCNP.
- I Number of predictor steps—this is another variable affecting the accuracy of the results. As the isotopic composition of a material changes during an irradiation step (both due to burnup and potential variances in continuous feed from beginning to end), the cross-sections may change as well. To obtain the most accurate results, spectrum-averaged, one-group cross-sections for a burn step should represent an average over the time interval. In a monteburns calculation, ORIGEN2 is run halfway through each outer burn step, and the resulting isotopics are used in MCNP to calculate spectrum-averaged, one-group cross-sections and fluxes for that

step. Then a complete ORIGEN2 run is performed with the new values to determine final compositions. This assumes that the isotopics of the system at the midpoint are a reasonable approximation of the isotopics over the entire burn step, and that cross-sections are representative of the step (actually it is only important that the neutron flux energy spectrum be representative of the entire burn step). The user must be aware of this assumption and consequently ensure that burn intervals are not too long.

If the initial cross-sections for a step are not accurate, then the ORIGEN2 compositions halfway through the step may not be a good representation of the burn step. Thus, it is often beneficial to perform a "predictor" step (derived from a basic form of the predictor-corrector method) to calculate cross-sections more than once at the midpoint of a burn step and to compare the neutron energy spectrum and isotopic compositions halfway through the step (these values are printed in the output files) to make sure that the final cross-sections are representative of the system at that step. The number of times for which cross-sections are calculated halfway through each step is the number of predictor steps. Executing multiple predictor steps increases the accuracy of the burnup calculation because the spectrum-averaged, one-group cross-sections used to perform the predictor step approach the ones calculated by the predictor step (i.e., they converge). In addition, monteburns automatically adds a predictor step for the initial burn step because the actual spectrum-averaged, one-group cross-sections for a system may be different than those supplied in the chosen default ORIGEN2 library. This problem can be partially avoided by providing an initial library that has been previously generated by monteburns for a similar system instead of using one of the ORIGEN2 default libraries (see the "Identifier for ORIGEN2 library" bullet below for more information). For all subsequent burn steps, monteburns uses the modified spectrumaveraged, one-group cross-section library from the previous burn step; thus, an extra predictor step is not required.

• I Step to restart after—a user can use this parameter to restart a run that ends unexpectedly or to branch off from a previous monteburns run with different input variables (for example, if keff drops too low during the nth burn step, the user can change the feed rate for the nth step and restart from the previous step). The "restart step" indicates the outer burn step after which monteburns should start, using all previously created input files and results for the outer burn steps up to that point. To use this variable effectively, all input files that were created by monteburns during the previous run must remain in the tmpfile subdirectory of the directory in which monteburns previously ran. If a restart run is not being performed, then the "restart step" value should be zero. This value gets modified during each step to reflect the value of the current step. Monteburns appends data obtained from the restart run to the existing output files so that easier comparisons can be made. As a result, some of the

production/destruction data may not be accurate, and an "Abort" error will occur because it cannot be read correctly. This has no impact on the other results and should be ignored.

- Identifier for ORIGEN2 library—this identifies from which ORIGEN2 library initial cross-section values are obtained (they are modified to be system-dependent after the first step). The ORIGEN2 manual8 contains a list of over 30 different cross-section libraries for different types of systems from which the user can choose. Each of these libraries should have been provided with the source code from Radiation Safety Information Computational Center (RSICC) and is associated with either an orig## file, where ## is a number used to identify the library or a "name.lib" (or "NAME.LIB" in VMS), where "name" and "##" are identified in Table 4. Either the value of this two-digit number or the associated name (WITHOUT the .lib extension) must be entered by the user. If the user generates his/her own ORIGEN2 library (i.e., from a previous monteburns run) to be used as the initial library, he/she must give it a name (orig## or "name") that does not currently exist and place it in the proper library location (see below) and must reference it within the FORTRAN77 program (see the authors for more guidance about doing this).
- © ORIGEN2 library location—this line of input must contain the location of the ORIGEN2 libraries (both decay and cross-section) in the user's file space or in the directory of another user on the system that has the library files. This way, only one user on a UNIX operating system needs to have a copy of the libraries. The decay library must also appear in this location as orig21 (for the "##" input above) or Decay.lib/DECAY.LIB, along with the appropriate cross-section library(ies).
- I Importance fraction—this value represents the lower limit (tolerance) for the importance of one isotope relative to the rest of the system based on results obtained from ORIGEN2 and MCNP. If an isotope contributes a large enough fraction (i.e., greater than the importance fraction) to absorption or fission interactions, mass, or atom density (see Section 3.2.6 for more information), then the isotope is considered "important." Flux spectrum-averaged, cross-section tallies are then one-group, performed in MCNP for this isotope. If the importance fraction is zero, then all activation, fission products, and actinides generated in ORIGEN2 are tallied (except those for which no MCNP cross-section exists—see Section 3.3.4 for more information). If the importance fraction is one, then no isotopes are deemed "important" except those specified as "automatic" in the input. Additionally, it is advised that the initial ORIGEN2 library is somewhat representative of the system, or "important" isotopes may not be properly identified. The only way to absolutely avoid this problem is to track every isotope or to generate a problem-specific library with a

TABLE 4
INITIAL CROSS-SECTION LIBRARIES PROVIDED BY ORIGEN2

Library	Character Identifier (VMS)	Number Identifier (UNIX)
PWR: ²³⁵ U-enriched UO ₂ with a burnup of 33,000 MWd/MTU	PWRU	orig22
PWR: ²³⁵ U-enriched UO ₂ in a self-generated Pu recycle reactor	PWRPUU	orig23
PWR: Pu-enriched UO ₂ in a self-generated Pu recycle reactor	PWRPUPU	orig24
PWR: ThO ₂ -enriched with denatured ²³³ U	PWRDU3TH	orig25
PWR: ThO ₂ -enriched with recycled, denatured ²³³ U	PWRD5D33	orig26
PWR: ThO ₂ -enriched with makeup, denatured ²³⁵ U	PWRD5D35	orig27
PWR: Pu-enriched ThO ₂	PWRPUTH	orig28
PWR: ²³⁵ U-enriched UO ₂ with a burnup of 50,000 MWd/MTU	PWRU50	orig29
BWR: ²³⁵ U-enriched UO ₂	BWRU	orig30
BWR: ²³⁵ U-enriched fuel in a self-generated Pu recycle reactor	BWRPUU	orig31
BWR: Pu-enriched fuel in a self-generated Pu recycle reactor	BWRPUPU	orig32
Thermal: 0.0253 eV cross-sections	THERMAL	orig33
CANDU: Natural	CANDUNAU	orig34
CANDU: Slightly Enriched	CANDUSEU	orig35
LMFBR: Advanced Oxide, LWR-Pu/U/U/U Core	AMOPUUUC	orig36
Axial Blanket	AMOPUUUA	orig37
Radial Blanket	AMOPUUUR	orig38
LMFBR: Early Oxide, LWR-Pu/U/U/U Core	EMOPUUUC	orig39
Axial Blanket	EMOPUUUA	orig40
Radial Blanket	EMOPUUUR	orig41
LMFBR: Advanced Oxide, recycle-Pu/U/U/U Core	AMORUUUC	orig42
Axial Blanket	AMORUUUA	orig43
Radial Blanket	AMORUUUR	orig44
LMFBR: Advanced Oxide, LWR-Pu/U/U/Th Core	AMOPUUTC	orig45
Axial Blanket	AMOPUUTA	orig46
Radial Blanket	AMOPUUTR	orig47
LMFBR: Advanced Oxide, LWR-Pu/Th/Th Core	AMOPTTTC	orig48
Axial Blanket	AMOPTTTA	orig49
Radial Blanket	AMOPTTTR	orig50
LMFBR: Advanced Oxide, 14% denatured ²³³ U/Th/Th/Th Core	AMO1TTTC	orig51
Axial Blanket	AMO1TTTA	orig52
Radial Blanket	AMO1TTTR	orig53
LMFBR: Advanced Oxide, 44% denatured ²³³ U/Th/Th/Th Core	AMO2TTTC	orig54
Axial Blanket	AMO2TTTA	orig55
Radial Blanket	AMO2TTTR	orig56
LMFBR: Advanced Oxide, recycle- ²³³ U/Th/Th/Th Core	AMODTTTC	orig57
Axial Blanket	AMODTTTA	orig58
Radial Blanket	AMODTTTR	orig59
LMFBR: FFTF Pu/U	FFTFC	orig60
ATW (created by TSA-10 at LANL)	ATW	orig65

previous run of monteburns that replaces the original default ORIGEN2 library (see the "Identifier for ORIGEN2 library" bullet above for more information).

The user must also decide how to deal with fission products. If the user enters the importance fraction as a positive value, then only those fission products deemed "important" are included in MCNP. However, because MCNP cross-sections for many fission products do not exist, monteburns contains the option to lump all fission products together as one sum (except for those fission products, if any, designated as "automatic" in the monteburns input file) by using a negative value here. These lumped fission products are then given one of two general fission product crosssections in MCNP—the average fission product from ²³⁵U and the average fission product from ²³⁹Pu (these have the identifiers 45117 and 46119 respectively¹). The fraction of the total fission product mass separated into each category is determined by comparing the number of fissions that result from isotopes with an atomic number less than or equal to that of uranium (92) to those that occur in other transuranic actinides with an atomic number >92. Note: the use of this attribute has not been fully benchmarked or documented, and the 45117 and 46119 data may be inaccurate for many applications, so exercise caution when using it! However, by developing representative cross-sections for such fission products and naming them 45117 and/or 46119 (with extensions other than the MCNP ones of .90c and .90d), the user can have more control over the data and know exactly where it came from.

• I Intermediate flag—this flag indicates whether or not intermediate keff calculations are performed. Normally, MCNP is only run once per predictor step, and these runs occur half way through each outer burn step (i.e., half way through each irradiation period). However, it is often desired to obtain a value of $k_{\mbox{\scriptsize eff}}$ at the beginning and/or end of each burn step. When the value of this parameter is one, additional MCNP calculations are performed to determine keff Neither cross-sections nor fluxes are recalculated by MCNP for these runs, so ORIGEN2 results are not influenced. The only purpose of the "intermediate" MCNP calculations is to provide the value of keff at more than one point during each outer burn step to see how the system changes. When a discrete feed addition (see Section 3.3.3) occurs, three MCNP runs are performed for the step (at the beginning, middle, and end); otherwise, two MCNP runs are performed (at the middle and end) because the beginning value of k_{off} equals the ending value of k_{eff} from the previous step. If the value of this parameter is zero, then only one MCNP run is performed for each outer burn step (in the middle) regardless of whether or not the discrete feed occurs.

• Number and list of automatic tally isotopes for each material—this integer represents the number of isotopes/elements for which the user wants tallies to be performed in MCNP and results written to monteburns output files (i.e., automatic "important" isotopes). The user must then number identification the **MCNP** for each isotopes/elements (these can indicate library preference and/or temperature dependence). It also allows the user to use a cross-section not specified in the default cross-section file discussed in Section 5.4, mbxs.inp (i.e., the cross-section identifier listed here has precedence over the one in mbxs.inp). The current limit on the total sum of the isotopes in all materials combined is slightly above 9000.

4.3. Feed Input Parameters

The purpose of a feed input file in *monteburns* is to list the lengths of each time step, to vary the fraction of power generated by the system during each time step, to shuffle materials from one region to another, and/or to specify amounts of materials to add to or remove from the system during each outer burn step. The user can also specify continuous or discrete (all at one time) feed (addition of isotopes) and/or removal (of specified elements) for each material at each time step in this file. First, for each outer burn step and material (for most items), the user enters the following parameters:

- length of the irradiation (in days)
- I fraction of power produced relative to the total power entered in the monteburns input file
- I region in which each material is located
- I feed group (defined below)
- I feed rate(s) (both beginning and ending rates for continuous and a flag and a rate for discrete)
- I removal group numbers (positive for continuous feed, negative for discrete
- I removal fraction [the fraction of each element removed (e.g., a fractional removal of 0.9 means that 90% of the removal group is removed and 10% remains)].

5.0. DESCRIPTION OF INPUT FILES

This section describes the four input files that monteburns uses, including (1) the MCNP input file, (2) the monteburns input file, (3) the feed input file, and (4) a cross-section map.

5.1. MCNP Input File

To execute monteburns, the user must have enough knowledge of MCNP to create an MCNP input file for the system that he/she wishes to analyze using either the "kcode" or "sdef" source definition. There is no required format of this input file in monteburns, except that material and user tally numbers must not be >100 (this is to keep monteburns tallies from interfering with user input), and it must be executable in MCNP. Note: This means it must also have at least 30 active kcode cycles to produce enough results to be analyzed by MCNP and thus monteburns. Explicit use of source files (srctp) is not yet supported; the source must be defined in the MCNP input file. A simple MCNP input file is included as Appendix A, and a more complex one (that will include a multimaterial burn) is in Appendix C.

5.2. Monteburns Input File

Another file that the user must create is an input file describing parameters required for the operation of monteburns. These parameters were described in detail in Section 4.2 and are listed along with appropriate format specifications in Table 5. A corresponding, simple (no feed or intermediate $k_{\rm eff}$ calculations) monteburns input file to go with the MCNP input file in Appendix A is displayed in Appendix B; one corresponding to Appendix C is in Appendix D.

5.3. Feed Input File

The feed input file allows the user to add or remove different amounts of materials to the system during each outer burn step, vary the power produced during each time interval for an irradiation, and/or shuffle materials from one region to another. The format of a feed input file is free, so the user can enter as large of numbers for each variable as desired as long as there are spaces in between variables.

TABLE 5
DESCRIPTION OF MONTEBURNS INPUT FILE

Parameter	Format	Description	Example
72-character title	72-char.	Briefly identifies scenario.	ATW
			system
			w/Tc99
Operating	4-char	What operating system user is on:	UNSU
System		UNSU = UNIX Sun	
		UNHP = UNIX HP	
		PC = PC	
		VMS = VMS	
Number of	integer	Number of materials from MCNP the	3
MCNP materials		user wants to have burned. This	
		number must be <50.	
MCNP material	integer	The "m" number of the material(s) in	1
number		the MCNP input file for which a	5
		burnup analysis is desired (all cells with	10
		this material(s) will be burned).	
Material volume	real	Volume of cells in MCNP containing	0.0
(cc)		the aforementioned material number(s)	0.0
		(Note: if the user wants to use the	0.0
		volume calculated by MCNP, then 0.0	
		should be entered here).	
Power (in MWt)	real	This is the total nominal power	1000.0
		generated by the system represented in	
		the MCNP input file.	
Recoverable	real	If known, the recoverable energy per	-200.0
energy per		fission for the system (in MeV). (Note:	
fission (in MeV)		if no value is known, then the value	
		for ²³⁵ U preceded by a negative sign can	
		be entered, and the Q-value will be	
		determined using this number and the	
		fraction of other actinides present).	
Total number of	real	Indicates the length of time over which	0.0
days burned		the entire irradiation will occur (Note:	
		this value should be zero if a feed file is	
		used and non-zero if one is not used).	
Number of outer	integer	This value represents the number of	7
burn steps		times cross-section values for ORIGEN2	
_		are updated by MCNP. When a feed file	
		exists, it should be equal to the number	
		of feed steps that exist in the feed input	
		file.	
		file.	

TABLE 5 (cont)

	r	4 1 10.4	
		Additionally, each step may represent	
		the addition or removal of more	
		material, or it may just represent an	
		additional timestep in irradiation	
		periods. The number of outer burn steps	
		must be <100.	
Number of	integer	This value gives the number of intervals	40
internal burn		into which the main irradiation period	
steps		for each ORIGEN2 input file will be	
		divided. The more internal burn steps,	
		the more accurate the results from	
		ORIGEN2. If continuous feed is being	
		used, this value should be divisible by	
		10; otherwise, it should be divisible by 2.	
Number of	integer	Number of times MCNP and ORIGEN2	1
predictor steps	801	should be run halfway through each	-
productor steps		outer burn step (to correlate cross-section	
		values with the composition of the	
		system during burnup).	
Step to restart	integer	A value of 0 represents a new	0
after	integer	monteburns run. If it is greater than 0,	U
alter		then it indicates the number of a	
		previously completed step after which	
		new calculations will be performed.	
		Note: Files containing information up to	
		this outer burn step must already exist	
		(in the user's working directory under	
77 1 0	4.0	the subdirectory tmpfile).	00 700
Number of	10-	The two-digit identification number or	60, Fftfc,
ORIGEN2	char.	name associated with the initial	or FFTFC
library		ORIGEN2 cross-section library.	
ORIGEN2	72-	This is the path name of the ORIGEN2	C:\origen
library location	char.	libraries in the user's directory.	2 ∖libs
Fractional	real	This value is the tolerance criteria used	0.005
importance		by monteburns to determine which	
limit		isotopes from ORIGEN2 are "important"	
		(see Section 3.4.6). "Important" isotopes	
		are those for which the atom fraction,	
		weight fraction, fraction of absorption,	
		and/or fraction of fission in the overall	
		material is greater than the limit listed	
<u> </u>	l	U	

TABLE 5 (cont)

Flag for	integer	here. If this value is less than zero, then those fission products that are not "automatically important" are lumped together as a general fission product in MCNP. This value indicates whether or not	0
intermediate	meger	intermediate MCNP run(s) are desired. If	,
k _{eff} calculations		activated (=1) for discrete feed cases, MCNP	
eff care area area.		will be run three times per burn step to get	
		k _{eff} calculations before, after, and halfway	
		through the step. If continuous or no feed	
		exists, then MCNP is only run twice, once	
		halfway through and once between burn	
		steps. A value of 0 indicates only one	
		MCNP run, which occurs halfway through	
		each outer burn step.	
Number of	integer;	The number of isotopes for which the use	9
automatic tally	for	specifies he/she wants to obtain tallies (no	93237.55c
isotopes and a	each	matter what the fractional importance the	94238.50c
list of those	iso-	isotopes are). For each material, this	94239.55c 94240.50c
isotopes for each	tope:	number is then followed by a list of those	94240.50c
material	first a	isotopes according to their MCNP	94242.50c
	five	identifiers.	95241.50c
	digit		95242.50c
	integer;	Material 1	95243.50c 9
	then a	\	9 93237.55c
	period		94238.50c
	and a		94239.55с
	three	Material 5	94240.50c
	digit		94241.50c
	iden-		94242.50c 95241.50c
	tifier;		95241.50c 95242.50c
	9-char.		95243.50c
	total		9
			93237.55c
			94238.50c
		Matarial 10	94239.55c 94240.50c
		Material 10	94240.50c 94241.50c
			94242.50c
			95241.50c
			95242.50c
		_	95243.50c

5.3.1. Basic Information

The following information about each outer burn must be included in the first block of data:

- 1. Step number
- 2. Irradiation time for each step
- 3. Fraction of total power at which the system will be operating during each burn step
- 4. Region in which each material will be located for the step
- 5. What feed group will be added to each material for the step (0 means no feed)
- 6., 7. Two feed rate columns
- 8. Number of the removal group number containing the elements that should be removed from ORIGEN2 output
- 9. What fraction of each element in this removal group should be removed

Items 5-7 will be discussed as part of the feed information and 8-9 as part of the removal information.

5.3.2. Feed Information

These variables comprise nine columns of data (see Table 5), which are read in free format. For burn steps where there is continuous feed, the first feed column (item 6) represents the feed rate (g/day) at the beginning of the step, and the second column (item 7) represents the feed rate at the end of the step. The exact rate of feed for each internal burn step is then obtained by interpolating between the beginning and ending feed rates. If a value of -1.0 is entered in the first feed rate column, then it is assumed that the beginning feed rate for that step is equal to the value of the ending feed rate of the previous step (thus, -1.0 cannot be entered as the beginning feed rate for the first step because it requires a previous step to obtain complete information). If the value entered in the first feed rate column is -2.0, then it indicates that discrete, not continuous, feed is added to the system at the beginning of the current outer burn step for this material. The amount of discrete feed added is equal to the value entered the second column (in grams/day) times the number of days in the irradiation. In either case, the user must enter the number of the feed material group he/she is adding for each outer burn step, or 0 if he/she is not adding any material

5.3.3. Removal Information

Similarly, for the removal groups, the user must first enter the number of the removal group, followed by the fraction of each element in the removal group that should be removed (0.0 means that none of the element's inventory is removed, whereas 1.0 means the entire inventory of the designated elements is removed). If the removal group number is positive, then continuous removal occurs, whereas if it is negative, then discrete removal occurs. For discrete removal, monteburns edits the ORIGEN2 output file so that the desired fraction of the designated range(s) of elements is removed at the end of each outer burn step. For continuous feed, the fission products are removed by ORIGEN2 after the halfway predictor step as well as at the end of the burn step for each ORIGEN2 run. If the value of zero is entered for a feed or removal group, then no feed addition or removal occurs in that material during that outer burn step.

5.3.4. Feed Material Groups

The next block of information in the feed input file provides detailed data about the feed material groups. First, the user must list the number of feed material groups that he/she uses. Then, for each feed material group, he/she must list the number of isotopes in that feed group followed by identifiers for those isotopes and the mass fraction of feed each isotope contributes to the final feed material (these do not have to add up to one). The identifier includes the atomic number directly followed by the atomic mass number for each isotope (such as 92235 for ²³⁵U).

5.3.5. Removal Groups

The final block of information describes the removal groups. Again, the user must first list the number of removal groups. Then, for each removal group, the user must list the number of ranges of consecutive elements that the removal group contains, followed by the atomic numbers of the first and last elements that comprise each range (all isotopes of the specified elements are in the removal group; i.e., individual isotopes may not be removed). For example, 28 to 68 would mean that all elements between nickel and erbium would be removed (which would represent the majority of fission products). The two ranges 28 to 42 and 44 to 68 would mean that all fission products in this same range, except technetium (Z=43), would be removed. The range 43 to 43 would indicate that the only element being removed would be technetium. For continuous removal (a removal group number >0), the appropriate elements would be removed both after the halfway predictor step and at the end of the burn (simulating continuous removal). For discrete removal (a removal group number <0), the elements are removed only at the end of the burn step (simulating discrete removal). In addition, ORIGEN2 has several different categories of isotopes: activation products, actinides, and fission products. The removal option in monteburns allows only isotopes generated as fission products to be removed, or it allows isotopes to be removed from all three categories. If the first integer in the range is listed as a positive number, isotopes of the element(s) listed in the removal group would be removed from all three categories. However, if this first integer is negative, then only isotopes of that element(s) that has been produced as fission products would be removed (if a smeared region contains Zr clad, the user may wish to only process the Zr fission product from the waste while not removing the clad material).

5.3.6. Material Shuffling

Also in the feed input file, the user can specify if and/or how to shuffle materials between regions. Monteburns regions are defined according to the initial listing of MCNP materials to be burned in the *mbfile.inp* file. The volume (of the applicable MCNP cells) associated with the first MCNP material listed in the mbfile.inp file is designated as region 1, and so on. These region numbers remain unchanged throughout the entire calculation. The material contained in a monteburns region is given the same material number as the region number; for example, when the output refers to monteburns material 2, it refers to the material in region 2 for that burn step. Column 4 in the feed file input specifies which monteburns material is to be placed in each region prior to each burn step. In particular, the number in each region represents which region the current material was previously in. For example, if there are two regions to be burned, the first burn step would normally contain a "1" in column 4 for the first region and a "2" in column 4 for the second region; thus, the materials would remain as specified in the *mbfile.inp* file. If the user wants to exchange the materials between the two regions prior to the second burn-step, then he/she would enter a "2" in column 4 for the first region and a "1" in column 4 for the second region (again, regions are defined in the order in which volumes appear in the mbfile.inp file, and this same order must be followed in the feed input file).

5.3.7. Format of Files

Tables 6a and 6b display the format of two different feed input files. In the first example file (Table 6a), material is irradiated in region 1, moved from region 1 to region 2, and irradiated in region 2. Finally, the material is processed [all fission products except technetium (Tc) are removed and then transuranic actinides and Tc-99 are added and reinserted into region 1. For all but the first step, feed material is added to the batch before entering region one (implied by a -2.0 in the first feed rate column), and in each step material is removed when the batch is pulled from region two (indicated by a negative removal group number). All fission products with an atomic number between 10 and 59 (with the exception of Tc) are removed and any isotope with an atomic number of 60 or 92 is removed (be it activation product, actinide, or fission product). The second example file (Table 6b) models continuous feed/removal of materials. In this case, plutonium is continuously added (at a decreasing rate) over the first five steps, whereas Tc is continuously removed. The feed is added continuously in ORIGEN2 over the burn period, and removal is performed by ORIGEN2 halfway through and at the end of each burn step (which in most monteburns cases will effectively simulate continuous removal). The -1.0 in the first feed rate column means that the beginning feed rate of the current step is the same as the ending feed rate of the previous step. If the feed rates at the beginning and end of the burn steps are different, then the feed rate used by ORIGEN2 is interpolated between these two values. The final two steps in Table 6b

are at zero power, which allows the material to decay with no irradiation involved. In addition to Tables 6a and 6b, another sample feed input file is included in Appendix E (which corresponds to the MCNP and monteburns input files in Appendices C and D, respectively).

5.3.8. Constant Burn Cases

If the user wants to perform a constant power burn with no material feed or removal, then he/she does not need to create a feed input file. Instead, a simple irradiation calculation would be performed in ORIGEN2 for the total length of irradiation (in days) listed in the *monteburns* input file (this value must be non-zero for such a case). The length of each outer burn step would then equal this value divided by the number of outer burn steps input.

5.4. Cross-section Map

The identifiers used to recognize isotopes in MCNP are different than those in ORIGEN2. Thus, monteburns is designed to determine which identifiers to use for each code. In ORIGEN2, the identifier is simply the atomic number followed by the atomic mass number and a "0" for stable isotopes and a "1" for metastable ones. MCNP not only requires the atomic number and atomic mass number but also a cross-section identifier. A file containing a list of default MCNP identifiers for all isotopes used or potentially created by decay or irradiation processes must be present in the directory in which the user is running so that monteburns knows what cross-sections to use. Note: cross-section libraries for many fission products may not exist and obviously cannot be listed here; they are subsequently ignored. This file is named mbxs.inp and can either be provided by the user or obtained with the source code and modified by the user as necessary. Each isotope must be listed on a separate line, and the values input here override those in the MCNP input file but do not override the ones listed in the monteburns input file.

For any isotopes deemed "important" by monteburns that do not have a cross-section identifier in this file, monteburns gives a warning that the cross-section is not found, continues to use the default ORIGEN2 cross-section, and does not transfer the material to MCNP. The identifiers in this file can either be cross-section libraries provided by MCNP, or they can be ones generated by the user with ENDF libraries, the code NJOY, and/or from other sources. In addition, mbxs.inp must include the general fission product identifiers 45117(.90c) and 46119(.90c) for MCNP if the lump sum of fission products option is used (as discussed in Section 4.2). A sample mbxs.inp file is displayed in Appendix F.

27

Versions of NJOY are available at the Radiation Safety Information Computational Center (RSICC) as codes PSR-171 and PSR-355.

TABLE 6a
DESCRIPTION/EXAMPLE 1 OF FEED INPUT FILE

Step	Time	Fraction	Material	Feed	1st Feed	2 nd Fee		Removal	Removal
#	step	of	# in	Group	Rate	Rate		Group #	Group
	(days)	Power	Each	#	Column	Column			Fraction
1	100.00	1 000	Region	0	0.0	0.0		0	1.000
1	182.62	1.000	1	0	0.0	0.0		0	1.000
- 0	005.05	1 000	2	0	0.0	0.0		-1	1.000
2	365.25	1.000	2	1	-2.0	1250.0		0	1.000
3	547.87	1.000	1 2	0	0.0 -2.0	0.0		-1 0	1.000
3	547.87	1.000	2 1	0	-2.0 0.0	0.0		-1	1.000 1.000
4	730.50	1.000	2	1	-2.0	1070.0		0	1.000
4	730.30	1.000	1	0	$\frac{-2.0}{0.0}$	0.0		-1	1.000
5	730.50	1.000	2	1	-2.0	1050.0		0	1.000
Э	730.50	1.000	ے 1	0	-2.0 0.0	0.0		-1	1.000
		Varia	-	U		mat			
Nisses	CE		DIE .		i4	mat	1	Examp	oie
		d Materials			14		1		
	ch Feed N		1		• 4		1	0	
		opes in feed			i4		12		
			Mass Num			5,f9.7 43099 0.310000 93237 0.044916			
			ight fraction						
			Note: this					238 0.0140 239 0.5142	
horrer	ive to auc	i up to one	e. It can be f es. For ex	ractionate	eu			239 0.3142 240 0.2375	
			es. For ex t-hand colu					240 0.2373 241 0.0786	
			tive to eac					241 0.0780 242 0.0480	
			/day of each					242 0.0480 241 0.0514	
			in the first					242 0.000(
			lless of whe					243 0.0092	
	one or no		iicss of wiid	ther it au	13			243 0.000 <i>1</i>	
up to	one or no	t. <i>)</i>						244 0.0017	
Number of Removal Groups					i4		1		- ·
	For Each Removal Group:								
Number of Ranges for Group					i4		4		
Range(s) of Atomic Numbers for Removal Group							- 1	0 -42	
180	(-, 01110		101 110111					14 –59	
								60 60	
								2 92	

TABLE 6b EXAMPLE 2 OF FEED INPUT FILE

Step	Time	Fraction	Material	Feed	1st Feed	2 nd Feed	Removal	Removal
#	step	of	# in	Group	Rate	Rate	Group #	Group
	(days)	Power	Each	#	Column	Column		Fraction
	·		Region					
1	182.62	1.000	1	1	1400.0	1300.0	1	1.000
2	365.25	1.000	1	1	-1.0	1250.0	1	1.000
3	547.87	1.000	1	1	-1.0	1150.0	1	1.000
4	730.50	1.000	1	1	-1.0	1070.0	1	1.000
5	730.50	1.000	1	1	-1.0	1050.0	1	1.000
6	365.25	0.000	1	1	0.0	0.0	0	0.000
7	365.25	0.000	1	1	0.0	0.0	0	0.000
		Variab	ole		For	Format Example		
Numb	er of Feed	d Materials			i4		1	
For Ea	ach Feed N	Material:						
Numb	er of isot	opes in feed	d		i4		2	
Identi	fier/Weig	ht Fraction			i5,f9.7	-	4239 0.94	
					9	4240 0.06		
Numb	Number of Removal Groups						1	
For Ea	For Each Removal Group:							
Number of Ranges					i4		1	
Range	•			•	i4,i4		43 43	

6.0. ERROR MESSAGES

There are a number of problems that can occur in *monteburns*, some of which may be caused by errors in the user's input files. Many such errors are accompanied by warning or error messages that appear on the screen (with the exception of one, which appears in the file T9err_#) to notify the user of the potential problem(s). These messages are listed and described in Table 7.

TABLE 7 ERROR MESSAGES

Error Message	Cause
**** MB ERROR:	Different operating systems have different system-
You must uncomment	dependent calls for obtaining arguments on the command
certain lines at the top	line. This error occurs when the operating system specified
of the source code for	in input is not consistent with the FORTRAN executable (a
this operating system	compilation error should also occur in this case).
***** MB ERROR:	The monteburns input file was not read in correctly. Please
Problem with	check your file for formatting and try again.
monteburns input file	
**** MB ERROR:	If the user inputs a material volume of 0.0 in the ***.inp
No tally volume	file, then the volume of the MCNP material must be
	obtained by adding up the volume of each cell containing
	that material in the MCNP output file. If MCNP contains
	no value for any cells containing that material, then this
	error message will appear. Because this volume is used in
	energy spectrum and cross-section tally calculations,
	monteburns will terminate after displaying this error
	message if the volume is zero.
***** MB WARNING:	The MCNP cross-section libraries used in this program only
Natural iso xs not	have a limited number of values for natural elements. If
found #####	the natural element entered by the user is not found in the
	cross-section library used in this program, then this error
	message appears and the element will not be included in
	the MCNP input files. The cause of this error could either
	be that the user forgot to put the natural element cross-
	section in mbxs.inp or that it does not exist in MCNP (in
	which case the MCNP input file would not work anyway).
***** MB WARNING:	This warning message appears when the cross-section for
Iso xs not found	one of the isotopes originally found in the MCNP input file
#####	cannot be found in the file mbxs.inp (the user should add it
	to this file).
**** MB ERROR:	The ORIGEN2 library specified by the user (for initial cross-
Initial ORIGEN2	sections) was not found on the system (see Section 4.2.2).
library was not found	
***** MB ERROR:	In the feed input file, the user must enter the number of
Invalid removal group	the removal group associated with each outer burn step.
entered for outer step	Additionally, he/she must also enter the number of
number #	removal groups in the final block along with the atomic
	number of element ranges in the removal groups. If the
	user enters a removal group number greater than the value
	of the number of removal groups, then this error message

TABLE 7 (cont) ERROR MESSAGES

Error Message	Cause
	appears on the screen and monteburns stops running (# stands for the outer burn step number).
**** MB ERROR:	The feed input file was not read in correctly. Please check
Problem with feed	your file for formatting and try again.
input file	
**** MB ERROR:	In the monteburns input file (***.inp), the user must
Not all user-specified	specify which material(s) from MCNP he/she wishes to
MCNP materials were	have burned (i.e., transferred between ORIGEN2 and
found in MCNP	MCNP). If one or more of these materials are not found in
output file	the MCNP output file, then this error message will appear
	on the screen and monteburns will terminate
***** MB ERROR:	This means that the flux tally value from an MCNP output
Tally read error	file was read as zero. A flux value of zero is then
	transferred to an ORIGEN2 input file, which means that no
	burnup will occur. Nonetheless, monteburns does not stop
	running.
***** MB ERROR:	If there are not enough tally output results in the MCNP
Cross-section Tallies	output file for the number of tallies needed, then this error
Not Correct	message will occur. It typically indicates a problem with the
	MCNP run. This error could be caused by tallies that existed
	in the initial MCNP deck (if they were numbered >100), or
	if the user exceeds the maximum allowable material limits.
***** MB WARNING:	There are some fission and activation products produced
Isotope ##### not	during the irradiation of a material that do not have cross-
found in TAPE9.INP	section values in the working ORIGEN2 cross-section file.
	Thus, their fraction importance in the areas of absorption
	and fission contribution cannot be calculated (although
	atom and weight fraction are). These fission and activation
	products are listed with this warning message in the file
	"tmpfile/T9err_\$" (\$ is the monteburns material number).
***** MB WARNING:	Although not necessarily a concern, these should be noted.
	The MCNP cross-section libraries used in this program
mcnp xs not found #####	have a limited number of isotopes for which cross-section values exist. If an isotope is determined by monteburns to
	be "important," but its cross-section identifier for MCNP
	does not exist in the file mbxs.inp, then this warning
	message appears and the isotope is not transferred back to
	MCNP. This message may also appear if an isotope from a
	natural element in the initial MCNP input is found to be
	natural element in the initial vicini input is found to be

TABLE 7 (cont) ERROR MESSAGES

Error Message	Cause
	"important" but does not have a cross-section because it is a
	natural element. It is then typically included in the MCNP
	input file as part of the natural element.
***** MB WARNING:	If the fractional importance value is negative, then fission
No Uranium (or	products resulting from ORIGEN2 irradiation calculations
Plutonium) Fission	(except those deemed "important") are summed together
Product library was	and given two general MCNP cross-sections for fission
provided in mbxs.inp	products (the total sum is divided according to the percent
	of fissions caused by ²³⁵ Uand ²³⁹ Pu and given the
	appropriate cross-section for each). If either of these two
	fission product cross-section libraries are not included in
	mbxs.inp, then this message appears and they are neglected.

7.0. OUTPUT FILES

Two large, primary output files are produced by monteburns. These output files consist of the name of the MCNP input file created by the user followed either by the extension ".out" or ".chk." For each of the output groups listed below (except the first two, which contain system, not material dependent parameters), results appear for each monteburns material/region being analyzed. Note: this is not necessarily the same as the initial MCNP material number assigned to each region because of shuffling between regions. The user must keep track of each MCNP material individually through the various regions when shuffling occurs. A sample .out file is included as Appendix G.

The first output file, mbfile.out, contains the results displayed below for each outer burn step.

- I Monteburns MCNP k_{eff} Vs Time—a list of the cumulative time (in days) over which irradiation has occurred as well as the effective multiplication factor (k_{eff}), associated relative error, [Eqs. (8) or (9)], average recoverable energy per fission calculated by monteburns [Eqs. (1–4)], and for the system (Eq. 10).
- Monteburns MCNP k_{eff} at Beginning of Step—a list of the cumulative time of irradiation (in days) that has occurred before each step begins as well as the effective multiplication factor, relative error, and at the beginning of each outer burn step (after discrete feed occurs). These data

are only included in the output if discrete feed is used and intermediate $k_{\mbox{\tiny eff}}$ calculations are requested.

For each material and outer burn step, the following parameters are output.

The following results are provided for each "automatic" isotope in each material for each outer burn step

- **Monteburns** One-Group Fission Cross-sections—the value of the microscopic fission cross-section ($_{i}$).
- I Monteburns Fission-to-Capture Ratio—the ratio of the microscopic fission cross-section to the microscopic capture (n,) cross-section ($_{\rm f}$ /) [does not include (n,), (n,p), etc].
- I Monteburns Grams of Material at End of Steps—the amount of material (in grams) at the end of each step.
- • Monteburns Grams of Feed—the amount of material (in grams) added to the system.

- I Summary of Inventory/Feed/Production—the total amount of material in the system at the beginning and end of monteburns (not of each step), the amount added through feed, and the net change. The interpretation of these data may also depend on feed, removal, and/or material shuffling.
- **Feed Rate**—the average continuous feed rate (in grams per day).
- Production/Destruction Rate—the rate of change (in grams per day) of material produced to that destroyed during irradiation. The interpretation of these data may depend on feed, removal, or material shuffling.
- Monteburns Activity of Material at End of Steps—the activity (in Curies) of each isotope [Eq. (18)].
- I Monteburns Heatload of Material at End of Steps—the decay power (heatload in W) of each isotope (Eq. 20).

- I Feed Input File—if it exists, this file is included at the end of this output file so that the user can determine what feed parameters he/she used to produce the results presented in this output file.

In the second output file, mbfile. chk, many intermediate results from the execution of monteburns are listed. In this output file, the following results are reported for each monteburns material analyzed for each predictor step.

• • Monteburns Spectrum for Each Predictor—the percent of neutrons with energies in each of the following ranges: 0 to 0.1 eV, 0.1 to 1 eV, 1 to 100 eV, 100 eV to 100 keV, 100 keV to 1 MeV, and 1 to 20 MeV. This can be

used to determine if smaller time intervals or more predictor steps need to be run.

- Importance Fraction of Isotopes Sent from ORIGEN2 to MCNP—the isotopes deemed "important," both automatically and through the importance fraction. This list contains the total mass of the isotope in the specified region and the contribution of each isotope in the following four categories: absorption, fission, mass fraction, and atom fraction. For example, if the fission column for an isotope reads 0.1, then 10% of the overall fissions in the material resulted from this isotope. This file also includes a warning message if an isotope deemed "important" by monteburns or "automatic" by the user is not found in the MCNP cross-section library used by monteburns.

8.0. LIMITATIONS OF AND FUTURE WORK FOR MONTEBURNS

Monteburns is only as good as the MCNP cross-sections that are available to the user. If cross-section libraries do not exist for several fission products or actinides, or cross-sections at the appropriate temperatures are not available, then monteburns results should be closely scrutinized. Monteburns is also limited by the accuracy of the ORIGEN2 fission product yields.

 $\it Monteburns$ output only contains data relating to material isotopics and a few reactor physics parameters (k_{eff} , , etc.). It can be modified in the future, however, to extract more values, depending on what uses the program might eventually have.

Monteburns currently uses the most simple form of the predictor-corrector method. In the future a more sophisticated numerical technique could be applied, although the simple method has proven adequate for problems studied thus far.

Monteburns currently uses ORIGEN2.1. There may be some advantages to using ORIGEN-S or CINDER⁵ in the future because of increased output options, improved default cross-section sets and fission product yields, and possibly wider availability.

Monteburns cannot currently handle any neutron reaction other than (n,), (n,f), (n,2n), (n,3n), (n,), and (n,p). Any application that relies significantly on any other reaction [for example, (n,t) in Li^6] will not work correctly.

Monteburns does not currently work with the Lahet Code System (LCS) or MCNPX. For now, accelerator-driven systems need to be evaluated with a MCNP "sdef" source definition. Test problems have shown that an evaporation source with a proper geometric distribution produces results similar to a full-blown, high-energy neutron solution (for systems with reasonably high neutron multiplication). Because of the lack of high-energy capability, monteburns does not handle spallation products.

As mentioned in Section 3.4.1, monteburns could do a better job of calculating changes in Q_{fis} as the system burns. Future modifications may look at adding the necessary tallies to better estimate Q_{fis} (to include the energy deposition from fission gammas, capture gammas, and neutron kinetic energy).

More detailed benchmarking efforts also need to be performed. Although two-dimensional reactor systems have been benchmarked to SCALE runs, 9,3 three-dimensional systems need to be studied in more detail.

In addition to the possible modifications above, work is ongoing to make the input/output of monteburns more user-friendly. Also, work is continuing in the benchmarking of monteburns to experimental and analytical burnup results, as well as for a wide range of inputs.

Any problems not already addressed should be reported to the contacts in Section 1.1 so that they can be corrected.

9.0. IMPLEMENTATION OF MONTEBURNS

The *monteburns.pl* executable can be run on almost any platform as long as the following files are present in the working directory and the directory has access to Perl, MCNP, and ORIGEN2 (including the libraries). The symbol '*mbfile*' represents the name the user assigns to the input files (Note: all three input files must have the same name with different extensions).

- Mbfile—MCNP input file
- • mbfile.inp—user's input file
- I mbfile.feed (optional)—feed input file
- * mbxs.inp—MCNP cross-section file
- I monteb or monteb.exe (FORTRAN77 executable) and/or monteb.f (FORTRAN77 program)
- \square monteburns .pl—Perl script file

9.1. UNIX

To run monteburns.pl on a UNIX system, the user must have a copy of monteburns.pl and either the executable FORTRAN77 program monteb that is operable on his/her system or compile the executable from the FORTRAN77 program monteb.f. The FORTRAN77 program can be compiled using the following command.

% f77 -o monteb monteb.f

Note: when using an HP system, there are several lines at the beginning of the monteb.f file that must be commented out (these are clearly marked within the first 25 lines of *monteb.f*), and some that must be uncommented before it will compile.

Alternatively, an executable for both UNIX systems (Sun and HP) is available with the source code as *monteb* and *monteb*. hp respectively.

Monteburns can then be run by typing the following command at the UNIX prompt.

% monteburns.pl

If the user obtains a "permission denied" message, then make the file an executable with the following command.

% chmod +x monteburns.pl

Once it is running, the basename of the input files will be requested with the following line: "Enter base name of input files."

After entering this information (i.e., the name *mbfile*), *monteburns* should be running with messages printed to the screen telling the user at which step in execution he/she is. A log file of detailed information, *log.txt*, will also be produced, which is helpful in determining what went wrong in a "bad" run.

9.2. PC

Running monteburns on the PC is almost identical to UNIX except that the executable is called monteb.exe. If the user wishes to compile on the PC, then he/she must use a compiler that handles the "getarg" function (i.e., Digitial Developer Studio 5.0 or 6.0 or others, not Lahey). To run in a windows environment, the user can simply click on the executable monteburns.pl. In a DOS environment, the program can again be run by typing "monteburns.pl." Monteburns has been tested on a Windows NT platform and should work on other Windows systems, but this cannot be guaranteed.

9.3. VMS

Running monteburns on a VMS system is similar to UNIX except that again, there are several lines at the beginning of the monteb.f file that must be commented out and some that must be added (what is there for VMS may or may not work correctly). The details necessary for this system were not yet identified when this manual was published, so any user that wants to use this system may have to do a little manipulation. Please contact the authors during or after this process so the capability may become available to others (or check with RSICC to see whether or not it was done yet).

10.0. REFERENCES

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- 8. A. G. Croff, "A User's Manual for ORIGEN2 Computer Code," Oak Ridge National Laboratory document ORNL/TM-7175 (July 1980).
- 9. H. R. Trellue, "Development of Monteburns: a Code that Links MCNP and ORIGEN2 in an Automated Fashion for Burnup Calculations," Los Alamos National Laboratory document LA-13514-T (December 1998).

11.0. APPENDICES

51
57
58
61
62
63
66

See the enclosed appendices.

APPENDIX A - MCNP Input File - test1

```
Heatpipe power system - Nb1Zr clad UN, flat/flat=20.1cm. length=31cm
    Passively safe: radref on, drums in, flooded, wet sand surround
    Passively safe: radref off, flooded, wet sand surround
    Passively safe: radref off, flooded, water surround
101 0
                -401 402 -403 404 -405 406
                                               $ Core (fill=1)
                 203 -206 fill=1 imp:n=1
102 8
       -8.64
                -411 412 -413 414 -415 416
                                               $ Hex
                (401:-402:403:-404:405:-406)
                 203 - 206 \text{ imp:n=1}
                -441 442 -443 444 -445 446
103 0
                (411:-412:413:-414:415:-416)
                 203 -206 imp:n=1
110
        -8.64
                -411 412 -413
                               414 -415
                                          416
                                               206 -207
                                                         imp:n=1 $ Nb Plate
     8
                                          416
112 8 -8.64
                     412 -413
                                414 -415
                                               202 -203
                -411
                                                         imp:n=1 $ Nb plate
                     412 -413
                                414 -415
113
                -411
                                          416
                                               222 -202
                                                         imp:n=1 $ Void
    0
                                414 -415
114
    8
       -8.64
                -411 412 -413
                                          416
                                               201 -222
                                                          imp:n=1 $ Gamma Core
115
    8
       -8.64
                -250 200 -201
                                                          imp:n=1 $ Gamma ref
C
       Shield
C
120 12 -7.9
                -250 -260
                           199 -200
                                     imp:n=1 $ imp:p=4 $ SS Clad
121 20 -1.093
                -250 - 260
                           198 -199
                                     imp:n=1 $ imp:p=4 $ LiH
122 20 -1.093
                -250 -260
                           197 -198
                                     imp:n=1 $ imp:p=8 $ LiH
                                     imp:n=1 $ imp:p=8 $ LiH
123 20 -1.093
                -250 -260
                           196 -197
C
      124 5 -10.1
                      -250 -260 195 -196 imp:n=1 $ imp:p=16 $ W
С
C
124 20 -1.093
                -250 195 -196
                                    imp:n=1 $ imp:p=16 $ LiH
125 20 -1.093
                -250 -260
                          194 -195
                                     imp:n=1 $ imp:p=16 $ LiH
126 20 -1.093
                -250 -260
                          193 -194
                                     imp:n=1 $ imp:p=32 $ LiH
127 20 -1.093
                -250 -260
                                     imp:n=1 $ imp:p=32 $ LiH
                          192 -193
128 12 -7.9
                -250 -260
                          191 -192
                                     imp:n=1 $ imp:p=32 $ SS
131 0
                -250 -260
                          190 -191
                                     imp:n=1 $ imp:p=32 $ DummyVoidPastShield
                -250 260 -200 190
                                     imp:n=1 $ imp:p=32 $ Void outside taper
132 0
                                     imp:n=1 $ imp:p=32 $ Void to dose plane
133 0
                     -190
                           189 -104
134 0
                     -189
                           188 -104
                                     imp:n=1 $ imp:p=32 $ Void past dose plan
C
       Flood Zones
                (441:-442:443:-444:445:-446)
141
    0
                                               $ Void below RR
                -102 203 -213
                                 imp:n=1
                (441:-442:443:-444:445:-446)
142
     0
                                               $ Void above RR
                -102 -250 216 -206
                                      imp:n=1
                -102 -250 207 -208
143
     0
                                      imp:n=1
                                               $ Bot Flood
144
                (102:250) -103 201 -208
                                               $ Radial Flood
     0
                 #831 #832 #833 #834 #835 #836 imp:n=1
145
                (411:-412:413:-414:415:-416)
                                               $ Rad Plate Flood
     0
                  -102 -250 201 -203
                                        imp:n=1
146
                (411:-412:413:-414:415:-416)
                                               $ Rad Plate Flood
                  -102 -250 206 -207
                                        imp:n=1
C
       Kill Zones
С
151 0
                                      imp:n=0
                                                  $ Void outside shield cone
                 250 -103 190 -201
152 0
                 103 -104 190 -208
                                      imp:n=0
                                                  $ Void oustide flood zone
153 0
                 104:-188:208
                                      imp:n=0
C
      Rad Ref and Control
С
```

```
801
       -8.64
               -451 452 -453 454 -455 456 $ Nb1Zr RR Inner Liner
                (441:-442:443:-444:445:-446)
                213 -216 imp:n=1
802
                (248:101) -102 213 -216 -250 $ Nb1Zr RR Outer Liner
       -8.64
                #831 #832 #833 #834 #835 #836 imp:n=1
               -101 -248 213 -216 702 -703 #831 $ Rad Ref 1
811
       -2.86
                (451:-452:453:-454:455:-456)
                                             imp:n=1
812
    3
       -2.86
               -101 -248 213 -216 704 705 #832 $ Rad Ref 2
               (451:-452:453:-454:455:-456) imp:n=1
813
    3
       -2.86
               -101 -248 213 -216 702 -706 #833 $ Rad Ref 3
               (451:-452:453:-454:455:-456) imp:n=1
814
       -2.86
               -101 -248 213 -216 -701 704 #834 $ Rad Ref 4
               (451:-452:453:-454:455:-456) imp:n=1
815
       -2.86
               -101 -248 213 -216 -706 -703 #835 $ Rad Ref 5
    3
               (451:-452:453:-454:455:-456) imp:n=1
               -101 -248 213 -216 705 -701 #836 $ Rad Ref 6
816
    3
       -2.86
               (451:-452:453:-454:455:-456) imp:n=1
821
       -8.64
               -101 -248 701 -702 213 -216 $ Rad Ref Clad
               (451:-452:453:-454:455:-456) imp:n=1
822
    8
               -101 -248 703 -704 213 -216 $ Rad Ref Clad
       -8.64
               (451:-452:453:-454:455:-456) imp:n=1
               -101 -248 705 -706 213 -216 $ Rad Ref Clad
823
    8
       -8.64
               (451:-452:453:-454:455:-456)
                                             imp:n=1
824
       -8.64
               -101 -248 -701 702 213 -216 $ Rad Ref Clad
               (451:-452:453:-454:455:-456)
                                             imp:n=1
825
       -8.64
               -101 -248 -703 704 213 -216 $ Rad Ref Clad
                (451:-452:453:-454:455:-456) imp:n=1
               -101 -248 -705 706 213 -216 $ Rad Ref Clad
826
       -8.64
                (451:-452:453:-454:455:-456) imp:n=1
832
               -154 213 -214 fill=8 imp:n=1
                                                 $ Ctr Dm 1
833
    like 832 but *trcl=(0 0 0 60 30 90 150 60 90)
834
    like 832 but *trcl=(0 0 0 120
                                   30 90
                                          150 120 90)
    like 832 but *trcl=(0 0 0 180 90 90
                                           90 180 90)
835
    like 832 but *trcl=(0 0 0 120 150 90
                                           30 120 90)
836
    like 832 but *trcl=(0 0 0 60 150 90
831
                                           30 60 90)
С
851
    15 -2.30
               150 -151
                         155
                              156
                                     u=8 imp:n=1 $ B4C Ring
    66 -12.65
               151 -152
                         155
                              156
                                     u=8 imp:n=1 $ Mo/Re Ring
852
    15 -2.30
               152 -153 155 156
                                     u=8 imp:n=1 $ B4C Ring
853
854
    3 - 2.86
               -153 #851 #852 #853
                                     u=8 imp:n=1 $ Inner CD
855
                153
                                     u=8 imp:n=1 $ Gap
С
     Hex and Pins (or empty hexes)
C
201 0
                -301 302 -303 304 -305
                                          306
                 lat=2 u=1 imp:n=1
                  fill=-5:5 -5:5 0:0
              9 9 9 9 9 9 9 9 9 9
              9 9 9 9 9 4 2 4 4 4 9
              9 9 9 9 4 4 4 4 2 4 9
              9 9 9 4 2 4 2 4 4 4 9
              9 9 4 4 4 4 4 4 2 4 9
              9
               4 2 4 4 7 4 4 4 4 9
              9
               4 4 2 4 4 2 4 2 9 9
              9
               4 4 4 4 4 4 4 9 9 9
               2 4 2 4 2 4 9 9 9 9
              9 4 4 4 4 4 9 9 9 9 9
             9 9 9 9 9 9 9 9 9 9
С
```

```
UN Region HP
С
160
                               u=2 imp:n=1
                                            $ HP Void
                -511
                              u=2 imp:n=1
                                            $ Nb HP
161
                511 -503
    8 -8.64
168 17 -3.59
                              u=2 imp:n=1
                                            $ Interstitial
                 503
     UN Pin
                -501 204 -205 u=4 imp:n=1
180
    1 -13.56
                                            $ Fuel Pellet
    3 -2.86
                -501 -204
                              181
182 3 -2.86
               -501 205
                              u=4 imp:n=1
                                            $ Ax Ref Pellet
                501 -502
183 0
                             u=4 imp:n=1 $ Gap
184 7 -20.
                502 -504
                             u=4 imp:n=1
                                           $ Re Liner
185 8 -8.64
                504 -503
                             u=4 imp:n=1
                                            $ Nb Clad
192 17 -3.59
                 503
                              u=4 imp:n=1
                                            $ Interstitial
С
     Flux Trap
401
    0
                -512
                              u=7 imp:n=1
                                            $ Inner Void
402 15 -2.3
                512 -511
                              u=7 imp:n=1
                                            $ B4C
                 511 -503
                               u=7 imp:n=1
403
    6 -10.20
                                            $ Mo/Re Pipe
404 17 -3.59
                               u=7 imp:n=1 $ Interstitial
                 503
     BeO Pin
С
510
                -501
                              u=3 imp:n=1
                                            $ BeO Pellet
    3 - 2.86
511
    0
                 501 -502
                              u=3 imp:n=1
                                            $ Gap
                 502 -503
512 8 -8.64
                              u=3 imp:n=1
                                            $ Nb Clad
517 17 -3.59
                 503
                              u=3 imp:n=1 $ Interstitial
     Void, No Tube
601 8 -8.64
                -599
                             u=9 imp:n=1 $ Nb Slats
С
С
C
     Surface Cards
101
    cz 19.97
                 $ Rad Ref
102
        20.07
                 $ Nb-1Zr Liner
    CZ
103
    cz 40.55
                 $ Flood Plane
104 cz 185.00
                   $ Dose circle
С
                   $ Just past dose plane
188
    pz -1200.1
                   $ Dose plane
189 pz -1200.0
190 pz -72.40
                   $ Dummy void to allow tally
191 pz -71.40
                  $ SS Clad
192 pz -71.20
                  $ LiH
193
    pz -65.20
                   $ LiH
194
    pz -59.20
                  $ LiH
195
    pz -53.20
                  $ LiH
196
    pz - 47.20
                  $ LiH
    pz -41.20
197
                  $ LiH
198 pz -35.20
                  $ LiH
199 pz -30.20
                  $ SS Clad
200 pz -30.00
                  $ Thin gamma ref plate
201 pz -29.50
                  $ Thick gamma core
222 pz -27.50
                  $ Void
202 pz -21.50
                  $ Nb Plate
203 pz -21.00
                  $ Ax Ref
204 pz -16.00
                  $ Shield end of core
    pz 16.00
                  $ Nozzle end of core
205
    pz 21.00
206
                  $ Ax Ref
207
    pz 21.50
                  $ Nb Plate
208
    pz 34.00
                  $ Flood
213 pz -18.00
                  $ Bot Rad Ref
214 pz 16.00
                  $ Top of CD
216 pz 18.00
                  $ Top Rad Ref
```

```
248 kz 327.0 .0042 $ RR BeO Cone
250 kz 330.0 .0042 $ Dose Cone
260 kz -89.00 1.0 $ HP Cone
    Control Drum (120deg)
150 \, c/z \, 0
            15.72 2.75
151 c/z 0
             15.72 3.65
152 c/z 0 15.72 3.85
153 c/z 0 15.72 4.75
154 c/z 0 15.72 4.80
155 p -0.57735 1 0
                        15.72
156 p 0.57735 1 0
                        15.72
C
     Fuel pin hex
С
301 px 1.27
                               $ Flat to center
302 px -1.27
303 p .57735 1 0
                     1.46647
304 p .57735 1 0 -1.46647
305 p -.57735 1 0 1.46647
306 p -.57735 1 0 -1.46647
C
    Baffle inner planes
C
401 py 10.0688
402 py -10.0688
403 p 1.73205 1 0 20.1376
404 p 1.73205 1 0 -20.1376
405 p -1.73205 1 0 20.1376
406 p -1.73205 1 0 -20.1376
С
    2mm baffle planes
411 py 10.2688
412 py -10.2688
413 p 1.73205 1 0 20.5376
414 p 1.73205 1 0 -20.5376
415 p -1.73205 1 0 20.5376
416 p -1.73205 1 0 -20.5376
    RadRef Nb1Zr (1mm gap)
441 py 10.3688
442 py -10.3688
443 p 1.73205 1 0 20.7376
444 p 1.73205 1 0 -20.7376
445 p -1.73205 1 0 20.7376
446 p -1.73205 1 0 -20.7376
    Rad Ref
С
451 py 10.4688
452 py -10.4688
453 p 1.73205 1 0 20.9376
454 p 1.73205 1 0 -20.9376
455 p -1.73205 1 0 20.9376
456 p -1.73205 1 0 -20.9376
     Fuel pin dimensions
C
501 cz 1.1350 $ Pellet
502 cz 1.1500
                  $ Gap
503 cz 1.2699
                  $ Clad
504 cz 1.2100
                  $ Re Liner
511 cz 1.1501 $ Inner HP wall
512 cz 1.1100 $ B4C Flux Trap Liner
                  $ Empty Hex Shell
599 cz 1.9999
```

```
С
      Rays Defining Radref sections
C
701 py -.1
702 py .1
703 p -1.73205 1 0 -.2
704 p -1.73205 1 0
                      . 2
705 p 1.73205 1 0
                       . 2
706 p
        1.73205 1 0 -.2
С
     UN TD=14.123 / 96%=13.56 (97.6 enr)
C
     92235.50c 0.488 92238.50c 0.012 7014.50c 0.5 $UN
С
     BeO TD=3.01 / 95%=2.86
С
m3
    4009.50c 0.5 8016.50c 0.5
                                                 $BeO
mt3 beo.06t
C
     Mo-Re TD=10.20
С
    42000.50c 1.000
mб
                                                  $Mo
     75185.50c .120 75187.50c .180
C
C
     Mo-25Re TD=12.65
С
     42000.50c .750
                                                  $Mo25Re
     75185.50c .100 75187.50c .150
C
     Re TD=20
C
    75185.50c .4
m7
                     75187.50c .6
                                                 $Re
С
С
     Nb1Zr TD=8.64
    41093.50c .99 40000.56c .01
                                                 $Nb1Zr
m8
С
С
     H20
c m10 1001.50c 2 8016.50c 1
                                                    $ H2O
c mt10 lwtr.01
С
     Wet Sand TD=2.05 (63.636%quartz)
С
c m11 1001.50c 0.72727
                                                    $ Wet sand
        8016.50c 1.63636
С
       14000.50c 0.63636
С
c mt11 lwtr.01
С
m12 42000.50c -0.02
                                 $ 316L Stainless
    24000.50c -0.16
                                 $(7.9g/cc)
    26000.55c -0.72
    28000.50c -0.10
С
     B4C TD=2.3 (90%enr)
C
m15
     5010.50c .720
                                                $B4C
     5011.50c .080
     6000.50c .200
С
     Ints Mat 3\%B4C TD=7.98g/cc, 45\%=3.59g/cc
С
     41093.50c -.97 5010.50c -.0231 6000.50c -.0069
m17
C
С
     Natural LiH with about 5 Vol% SS
m20
     42000.50c 8.4e-5
                                   $
     24000.50c 6.7e-4
     26000.55c 3.02e-3
```

```
28000.50c 4.2e-4
      1001.50c
                .05326
                3.994e-3
      3006.50c
      3007.50c
                0.04926
С
      Flooded Ints Mat 3%B4C 45%Nb+55%H20=4.14g/cc
С
С
  m97
         41093.50c -.8410 5010.50c -.0200 6000.50c -.0060
С
         1001.50c -.015
                          8016.50c -.118
         lwtr.01
С
  mt97
С
print
prdmp 100 5 0 1
mode n
kcode 1000 1.0 5 55
ksrc 6 0 9 6 0 -9 -6 0 9 -6 0 -9
```

End of Appendix A

APPENDIX B - Monteburns Input File With No Feed- test1.inp

```
Heatpipe Power System (HPS) 12 module core, 10 yr burn @ 750 kW
         ! Type of Operating System
UNSU
1
          ! Number of MCNP materials to burn
          ! MCNP material number #1 (will burn all cells with this mat)
1
          ! Material #1 volume (cc), input 0 to use mcnp value (if exists)
6022.
         ! Power in MWt (for the entire system modeled in mcnp deck)
         ! Recov. energy/fis (MeV); if negative use for U235, ratio other isos
-200.
3652.0
          ! Total number of days burned (used if no feed)
         ! Number of outer burn steps
40
          ! Number of internal burn steps (multiple of 10)
          ! Number of predictor steps (+1 on first step), 1 usually sufficient
          ! Step number to restart after (0=beginning)
Ω
          ! number of default origen2 lib - next line is origen2 lib location
/export/gus2/origen/libraries
.001 ! fractional importance (track isos with abs,fis,atom,mass fraction)
          ! Intermediate keff calc. 0) No 1) Yes
          ! Number of automatic tally isotopes, followed by list.
92235.50c
92238.50c
94239.55c
94240.50c
94241.50c
94242.50c
```

End of Appendix B

APPENDIX C - MCNP Input File - test5

(Note: this is the same as the "test3" file included with the source code but has better statistics (i.e., processes more particles), so results will vary somewhat)

```
Advanced ATW, 2mDiamx2mHigh, 2 GW, 0.5mTarg, Equil,
       Fuel - PWR mix
С
С
100
        2 -10.242
                  100 -120 -204
                                        imp:n=1
                                                        $ Lead
120
        2 -10.242
                  120 -130 -200
                                        imp:n=1
                                                        $ Lead Below Target
140
        2 -10.242
                  130 -131 421 -200
                                        imp:n=1
                                                        $ Lead Target
141
        2 -10.242 130 -131 -421
                                        imp:n=1
                                                       $ B4C Insert
150
       20 -7.9
                   131 -132 -200
                                        imp:n=1
                                                       $ Target Window
                   132 -160 421 -200
                                        imp:n=1
                                                       $ Void Above Lead
260
Target
261
                   132 -160 -421
                                        imp:n=1
                                                       $ B4C Insert
280
        2 -10.242
                  120 -140
                            203 -204
                                        imp:n=1
                                                        $ Lead
400
        2 -10.242
                  140 -160
                            200 -204
                                        imp:n=1
                                                       $ Lead
                                                       $ Fuel
420
       61 0.04284 120 -140
                            200 -201
                                        imp:n=1
       63 0.04284 120 -140
                            201 -202
                                        imp:n=1
                                                       $ Fuel
440
460
       64 0.04284 120 -140 202 -203
                                        imp:n=1
                                                       $ Fuel
       0 -100:160:204
                                        imp:n=0
999
                                                        $ Void
100
       pz -350.0
120
       pz -100.0
130
           -40.0
       pz
131
       pz
            15.0
132
       pz
            16.0
140
       pz
            100.0
160
       pz 350.0
C
200
       cz 25.0
201
       cz 61.237
       cz 82.916
202
203
       cz 100.0
204
       cz 400.0
421
       cz 24.99
m2
       82000.50c 0.445
                                           $ LBE, TD@400C=10.242 g/cc
       83209.50c 0.555
C
m20
      40000.56c -0.0001 $ Croloy 1.25, from Maria and Ann-Louise
      12000.50c -0.0035
      6000.50c -0.001
      25055.50c -0.004
      14000.50c -0.003
      24000.50c -0.0125
      42000.50c -0.006
      26000.55c -0.9699
c pwr1
        92238.50c 1.902E-04
m61
        93237.55c 3.454E-05
        94238.50c 1.073E-05
        94239.55c 3.922E-04
        94240.50c 1.805E-04
        94241.50c 5.951E-05
```

```
94242.50c 3.617E-05
        95241.50c 3.889E-05
        95242.50c 4.755E-08
        95243.50c 6.952E-06
        96243.35c 2.853E-08
        96244.50c 1.341E-06
        43099.50c 4.284E-04
        40000.56c 7.189E-03
        82000.50c 7.166E-03
        83209.50c 8.938E-03
        22000.50c 2.504E-05
        24000.50c 3.675E-03
        26000.50c 1.409E-02
        28000.50c 3.052E-03
        42000.50c 3.734E-04
c pwr2
m63
        92238.50c 2.125E-04
        93237.55c 3.859E-05
94238.50c 1.198E-05
        94239.55c 4.381E-04
        94240.50c 2.016E-04
        94241.50c 6.648E-05
        94242.50c 4.040E-05
        95241.50c 4.344E-05
        95242.50c 5.312E-08
        95243.50c 7.766E-06
        96243.35c 3.187E-08
        96244.50c 1.498E-06
        43099.50c 4.284E-04
        40000.56c 7.077E-03
        82000.50c 7.166E-03
        83209.50c 8.938E-03
        22000.50c 2.504E-05
        24000.50c 3.675E-03
        26000.50c 1.409E-02
        28000.50c 3.052E-03
        42000.50c 3.734E-04
print
       6.032e-8 12r
tmp
      Cell 141 is source
       2000
nps
С
     Source, d3=5 - evaporation spectrum, d1 gives parabolic
С
     distribution with radius of 24.9 cm, d2 gives cubic dist
С
     from -40 to 15 cm (top of target)
C
sdef par=1 erg=d3 pos=0 0 -40 axs=0 0 1 rad=d1 ext=d2
sp1 -21 0.
sil 24.9
c sp2 -31 0.0667
sp2 -21 3.
si2 0. 54.99
sp3 -5
dbcn
       12j 7.01e7
c pwr3
m64
        92238.50c 2.279E-04
        93237.55c 4.139E-05
        94238.50c 1.285E-05
```

```
94239.55c 4.699E-04
94240.50c 2.162E-04
94241.50c 7.130E-05
94242.50c 4.334E-05
95241.50c 4.660E-05
95242.50c 5.698E-08
95243.50c 8.330E-06
96243.35c 3.419E-08
96244.50c 1.607E-06
43099.50c 4.284E-04
40000.56c 7.000E-03
82000.50c 7.166E-03
83209.50c 8.938E-03
22000.50c
           2.504E-05
24000.50c
           3.675E-03
26000.50c 1.409E-02
28000.50c 3.052E-03
42000.50c 3.734E-04
```

End of Appendix C

APPENDIX D - Monteburns Input File - test5.inp

```
advlc Advanced ATW, 2mDiamx2mHigh, 2 GW, 0.5mTarg, Equil, with Tc-99 in fuel
             ! Type of Operating System
UNSU
3
             ! Number of MCNP materials
61
             ! MCNP Material number (must be less than 100)
             ! MCNP Material number
63
            ! MCNP Material number
             ! Material volume #1 (cc), input 0 to use mcnp value (if exists)
0.
0.
             ! Material volume #2
             ! Material volume #3
0.
2000.
            ! Power in MWt (for the entire system modeled in mcnp deck)
            ! Recov. energy/fission (MeV); if negative use for U235, ratio other isos ! Total number of days burned (used if no feed)
-200.
0.
            ! Number of outer burn steps
             ! Number of internal burn steps (multiple of 10)
! Number of predictor steps (+1 on first step), 1 usually sufficient
40
1
             ! Step number to restart after (0=beginning)
60
             ! Number of origen2 library - next line is origen2 lib. location
/export/gus2/origen/libraries
          ! fractional importance (track isos with abs,fis,atom,mass fraction)
.005
1
             ! Intermediate keff calc. 0) No 1) Yes
14
             ! Number of automatic tally isotopes, followed by list.
92238.50c
93237.55c
94238.50c
94239.55c
94240.50c
94241.50c
94242.50c
95241.50c
95242.50c
95243.50c
96242.50c
96243.35c
96244.50c
43099.50c
14
92238.50c
93237.55c
94238.50c
94239.55c
94240.50c
94241.50c
94242.50c
95241.50c
95242.50c
95243.50c
96242.50c
96243.35c
96244.50c
43099.50c
14
92238.50c
93237.55c
94238.50c
94239.55c
94240.50c
94241.50c
94242.50c
95241.50c
95242.50c
95243.50c
96242.50c
96243.35c
96244.50c
43099.50c
```

End of Appendix D

APPENDIX E - Feed Input File - test5.feed

Time	Days				_			Fraction	F.P.Removed
Step	Burned			#	_	ms/day	Group#		
1	121.76	1.000	1	0	0.0	0.0	-1	0.990 !	
			2	0	0.0	0.0	0	0.000 !	
			3	0	0.0	0.0	0	0.000 !	
2	121.76	1.000	2	0	0.0	0.0	-1	0.990 !	
			3	0	0.0	0.0	0	0.000 !	
			1	1	-2.0	3300.0	0	0.000 !	
3	121.76	1.000	2	0	0.0	0.0	-1	0.990 !	
			3	0	0.0	0.0	0	0.000 !	
			1	1	-2.0	2900.0	0	0.000 !	
4	121.76	1.000	2	0	0.0	0.0	-1	0.990 !	
			3	0	0.0	0.0	0	0.000 !	
			1	1	-2.0	2650.0	0	0.000 !	
1					! #	of feed s	pecs		
13						_		TC-99, L	WR Discharge
43099	.05500	0					. ,	,	
92238	.25000								
93237	.04491	6							
94238	.01400								
94239	.51421								
94240	.23759								
94241	.07868								
94242	.04801								
95241	.05142								
95242	.00006								
95243	.00926	_							
96243	.00003								
96244	.00179								
1	.00175	,			1 #	of removal	laroung	2	
3									oval sten
-10 -	-42					t range for			ovar sccp
-44						d range fo			
92	92					d range fo			
ラム	24				: 31	u range ro	or reed	# ⊥	

End of Appendix E

APPENDIX F - Sample MCNP Cross-section Map - mbxs.inp

1001.50c 1002.55c 1003.50c 2003.50c 2004.50c 3006.50c 3007.55c 4007.35c 4009.50c 5010.50c 5011.56c 6012.50c 6013.35c 6000.50c 7014.50c 7015.55c 8016.50c 9019.50c 11023.50c 12000.50c 13027.50c 14000.50c 15031.50c 16000.60c 16032.50c 17000.50c 18000.50c 19000.50c 20000.50c 21045.55c 22000.50c 23051.31c 23000.50c 24000.50c 25055.50c 26000.55c 27059.50c 28058.35c 28000.50c 29000.50c 31000.50c 33074.35c 33075.35c 35079.55c 35081.55c 36078.50c 36080.50c 36082.59c 36083.59c 36084.59c 36086.59c 37085.55c 37087.55c 39088.35c 39089.35c

40093.50c

40000.56c 41093.50c 42095.50c 42000.50c 43099.50c 44101.50c 44103.50c 45103.50c 45105.50c 46105.50c 46108.50c 47107.50c 47109.50c 47000.55c 48000.50c 50000.35c 53127.55c 53135.50c 54131.50c 54134.35c 54135.50c 54000.35c 55133.50c 55135.50c 56138.50c 59141.50c

62149.50c 62150.50c 62151.50c

60143.50c 60145.50c 60147.50c 60149.50c 61147.50c 61148.50c 61149.50c 62147.50c

- 62152.50c
- 63151.55c 63152.50c
- 63153.55c 63154.50c
- 63155.50c
- 63000.35c 64152.52c
- 64154.50c
- 64155.50c
- 64156.50c 64157.50c
- 64158.50c
- 64160.50c
- 64000.35c 67165.55c
- 69169.55c
- 72000.50c
- 73181.50c
- 74182.55c
- 74183.55c

74184.55c 74186.55c 74000.55c 75185.35c 75187.35c 77000.55c 78000.35c 79197.56c 82000.50c 83209.50c 90231.35c 90232.50c 90233.35c 91231.50c 91233.50c 92233.50c 92234.50c 92235.50c 92236.50c 92237.50c 92238.50c 92239.35c 92240.35c 93235.35c 93236.35c 93237.55c 93238.35c 94237.35c 94238.50c 94239.55c 94240.50c 94241.50c 94242.50c 94243.35c 95241.50c 95242.50c 95243.50c 96242.50c 96243.35c 96244.50c 96245.35c 96246.35c 96247.35c 96248.35c 97249.35c 98249.35c 98250.35c 98251.35c 98252.35c

End of Appendix F

End of Manual